

The following clarifications are provided based on questions received or changes in District requirements and must be added/considered when completing your submittal: Acknowledgement of receipt of this <u>ADDENDUM</u> is required in the proposal's cover letter of introduction. Please clearly note the addendum date and number.

ITEM:

A. CHANGES TO PROJECT MANUAL

NONE

B. CHANGES TO DRAWINGS

ITEM 1: Replace the bid drawing set in its entirety with the attached set of plans.

C. GEOTECHNICAL ENGINEERING REPORT

ITEM 1: Terracon Geotechnical Report

CODE SUMMARY & REGULATIONS	
AS A FACILITY WHICH COMES UNDER THE APPROVAL AND AUTHORITY OF THE DIVISION OF THE STATE ARCHITECT OFFICE OF REGULATION SERVICES (DSA), THIS PROJECT IS SUBJECT TO DRAWING AND JOB SITE REVIEW BY A REPRESENTATIVE OF DSA.	
 ADMINISTRATIVE REQUIREMENTS (PARTIAL LISTING ONLY FROM CHAPTER 4, PART 1, TITLE 24, C.C.R) A COPY OF PARTS 1 AND 2, TITLE 24, C.C.R. AND ALL SECTIONS OF THE CALIFORNIA BUILDING CODE (9 VOLUMES) SHALL BE KEPT ON SITES AT ALL TIMES. ALL CHANGE ORDERS AND ADDENDA TO BE SIGNED BY THE ARCHITECT OF RECORD AND THE OWNER AND APPROVED BY DSA. ALL SUBSTITUTIONS TREATED AS CHANGE ORDERS ARE NOT VALID UNTIL APPROVED BY DSA PER SECTION 4-333, PART 1, TITLE 24 DSA SHALL BE NOTIFIED AT THE START OF CONSTRUCTION AND PRIOR TO THE PLACEMENT OF CONCRETE PER SECTION 4-331, PART 1, TITLE 24 INSPECTOR SHALL BE APPROVED BY DSA AND EMPLOYED DIRECTLY BY OWNER. INSPECTION SHALL BE IN ACCORDANCE WITH SECTION 4-331(B), PART 1, TITLE 24 SUPERVISION OF CONSTRUCTION BY DSA SHALL BE IN ACCORDANCE WITH SECTION 4-334, PART 1, TITLE 24 CONTRACTOR, INSPECTOR, ARCHITECT OF RECORD AND ENGINEER SHALL SUBMIT VERIFIED REPORTS (DSA 6AE) IN ACCORDANCE WITH SECTION 4-336 AND 4-343, PART 1, TITLE 24 THE ARCHITECT OF RECORD AND STRUCTURAL ENGINEER SHALL PERFORM THEIR DUTIES IN ACCORDANCE WITH SECTION 4-336 (AND 4-343, PART 1, TITLE 24 THE CONTRACTOR SHALL PERFORM HIS DUTIES IN ACCORDANCE WITH SECTION 4-333, PART 1, TITLE 24 THE CONTRACTOR SHALL PERFORM HIS DUTIES IN ACCORDANCE WITH SECTION 4-333, PART 1, TITLE 24 THE CONTRACTOR SHALL PERFORM HIS DUTIES IN ACCORDANCE WITH SECTION 4-333, PART 1, TITLE 24 THE INTENT OF THE DRAWINGS AND PROJECT MANUAL IS THAT THE WORK OF THE ALTERATION, REHABILITATION OR RECONSTRUCTION SIN ADD REDSES BY ALL CONTRACT DOCUMENTS AND AFFECTING COMPLYING CONSTRUCTION SON ADDRESSED BY THE CONTRACT DOCUMENTS AND AFFECTING COMPLIANCE OF FINISHED WORK, ACHARGE ORDER OR SEPARATE SET OF CONSTRUCTION SUPON DISCOVERY OF NON-COMPLYING EXISTING CONDITIONS NOT ADDRESSED BY THE CONTRACT DOCUMENTS AND AFFECTING COMPLIANCE OF FINISHED WORK, A CHANGE ORDER OR SEPARATE SET OF CONSTRUCTION DOCUMENTS ADDRESSING THE NECESSARY REMEDIAL SLOPE OF	HORT
GOVERNING CODES	CONSULTANTS
*2013 CALIFORNIA BUILDING STANDARD, TITLE 24, PART 1 *2013 CALIFORNIA BUILDING CODE, TITLE 24, PART 2 *2013 CALIFORNIA ELECTRICAL CODE, TITLE 24, PART 3 *2013 CALIFORNIA MECHANICAL CODE, TITLE 24, PART 4 *2013 CALIFORNIA PLUMBING CODE, TITLE 24, PART 5 *2013 CALIFORNIA ENERGY CODE, TITLE 24, PART 6 *2013 CALIFORNIA FIRE CODE, TITLE 24, PART 9	STRUCTURAL ENGINEER:
 *2013 CALIFORNIA EXISTING BUILDING CODE, TITLE 24, PART 10 *2013 CALIFORNIA GREEN BUILDING STANDARD, TITLE 24, PART 11 *2013 CALIFORNIA BUILDING STANDARDS, TITLE 24, PART 12 *2013 NFPA 13-13 AUTOMATIC SPRINKLER SYSTEMS, WITH 2013 CBC AMENDMENTS *2013 NFPA 14-13 INSTALLATION OF STANDPIPE, PRIVATE HYDRANT AND HOSE SYSTEMS, WITH 2013 CBC AMENDMENTS *2013 NFPA 72-13 NATIONAL FIRE ALARM CODE, WITH 2013 CBC AMENDMENTS *2013 NFPA 20-13 INSTALLATION OF STATIONARY PUMPS FOR FIRE PROTECTION *2013 NFPA 22-13 WATER TANKS FOR PRIVATE FIRE PROTECTION *2013 NFPA 24-13 INSTALLATION OF PRIVATE FIRE SERVICE MAINS AND THEIR APPURTENANCES, WITH 2013 CBC AMENDMENTS *2013 NFPA 24-13 INSTALLATION OF PRIVATE FIRE SERVICE MAINS AND THEIR APPURTENANCES, WITH 2013 CBC AMENDMENTS *2008 NFPA 25 INSPECTION, TESTING, MAINTENANCE OF WATER-BASED FIRE PROTECTION SYSTEMS *2008 NFPA 25 INSPECTION, TESTING, MAINTENANCE OF WATER-BASED FIRE PROTECTION SYSTEMS *2007 ICC 300-12 STANDARDS ON BLEACHERS, FOLDING TELESCOPIC SEATING & GRANDSTANDS *2013 NFPA 17-13 DRY CHEMICAL EXTINGUISHING SYSTEMS *2013 NFPA 17A-13 WET CHEMICAL EXTINGUISHING SYSTEMS 	MECHANICAL ENGINEER:
 *2008 NFPA 2001-12 CLEAN AGENT FIRE EXTINGUISHING SYSTEMS *ASTM STANDARDS CHANGES (EXAMPLE: ASTM E648-04 STANDARD TEST METHOD FOR CRITICAL RADIANT FLUX OF FLOOR) *UL STANDARD CHANGES (EXAMPLE: 2005 UL 38 MANUAL OPERATING SIGNAL BOXES) *TITLE 24-12 CCR STATE FIRE MARSHAL REGULATIONS *2003 UL 464-03 AUDIBLE SIGNAL APPLIANCES *1999 UL 521-99 HEAT DETECTORS FOR FIRE PROTECTIVE SIGNALING SYSTEMS *2002 UL 1971 SIGNALING DEVICES FOR HEARING IMPAIRED *ADA STANDARDS FOR ACCESSIBLE DESIGN: 2010 ADA ACCESSIBILITY GUIDELINES (ADAAG) 28, PART 36 APPENDIX A *ADA STANDARDS FOR ACCESSIBLE DESIGN-CODE OF FEDERAL REGULATIONS (INCLUDING AMENDMENTS) * AISC MANUAL OF STEEL CONSTRUCTION, 14TH EDITION *2005 REVISED NATIONAL DESIGN SPECIFICATION FOR WOOD CONSTRUCTION *ACI 318-11 CODE AND COMMENTARY 	WATER INTRUSION CONSULTANT:
EQUIPMENT ANCHORAGE NOTES	SYMBOLS
 ALL MECHANICAL, PLUMBING AND ELECTRICAL COMPONENTS SHALL BE ANCHORED AND INSTALLED PER DETAILS ON DSA APPROVED CONSTRUCTION DOCUMENTS. WHERE NO DETAIL IS INDICATED, THE FOLLOWING COMPONENTS SHALL BE ANCHORED OR BRACED TO MEET THE FORCE AND DISPLACEMENT REQUIREMENTS PRESCRIBED IN 2013 CBC, SECTIONS 1615A.1.12 THROUGH 1615A.1.22 AND ASCE7-05 CHAPTER 6 AND 13: 1. ALL PERMANENT EQUIPMENT AND COMPONENTS 2. TEMPORARY OR MOVABLE EQUIPMENT THAT IS PERMANENTLY ATTACHED (E.G. HARD WIRED) TO THE BUILDING UTILITY SERVICES SUCH AS ELECTRICITY, GAS OR WATER. 3. MOVABLE EQUIPMENT WHICH IS STATIONED IN ONE PLACE FOR MORE THAN 8 HOURS AND HEAVIER THAN 400 POUNDS ARE REQUIRED TO BE ANCHORED WITH TEMPORARY ATTACHMENTS. THE ATTACHMENT OF THE FOLLOWING MECHANICAL AND ELECTRICAL COMPONENTS SHALL BE POSITIVELY ATTACHED TO THE STRUCTURE, BUT NOT BE DETAILED ON THE PLANS. THESE COMPONENTS SHALL HAVE FLEXIBLE CONNECTIONS	A STUDIO 1 COLUMN GRID LINE Numbers horizontal Letters vertical ROOM ID Room name & number C.13 A DOOR SYMBOL Door number
 PROVIDED BETWEEN THE COMPONENTS AND ASSOCIATED DUCTWORK, PIPING AND CONDUIT: COMPONENTS WEIGHING LESS THAN 400 POUNDS AND HAVE A CENTER OF MASS LOCATED 4 FEET OR LESS ABOVE THE ADJACENT FLOOR OR ROOF LEVEL THAT DIRECTLY SUPPORT THE COMPONENT. COMPONENTS WEIGHING LESS THAN 20 POUNDS, OR IN THE CASE OF DISTRIBUTED SYSTEMS, LESS THAN 5 POUNDS 	CT-1 <u>CT-1</u> <u>WINDOW SYMBOL</u> Window number <u>FINISH SYMBOL</u> Finish mat'l identification
PER FOOT, WHICH ARE SUSPENDED FROM A ROOF OR FLOOR OR HUNG FROM A WALL. FOR THOSE ELEMENTS THAT DO NOT REQUIRE DETAILS ON THE APPROVED DRAWINGS, THE INSTALLATION SHALL BE SUBJECT TO THE APPROVAL OF THE STRUCTURAL ENGINEER OF RECORD AND THE DSA DISTRICT STRUCTURAL ENGINEER. THE PROJECT INSPECTOR SHALL VERIFY THAT ALL COMPONENTS AND EQUIPMENT HAVE BEEN ANCHORED IN ACCORDANCE	10 A5.02 Section identification Sheet number
WITH THE ABOVE REQUIREMENTS. PIPING, DUCTWORK AND ELECTRICAL SYSTEM DISTRIBUTION SYSTEM BRACING NOTE DIDING, DUCTWORK AND ELECTRICAL DISTRIBUTION SYSTEMS SHALL BE REACED TO COMPLY WITH THE EORGES AND	10 A9.03 DETAIL REFERENCE Detail information Sheet number
PIPING, DUCTWORK AND ELECTRICAL DISTRIBUTION SYSTEMS SHALL BE BRACED TO COMPLY WITH THE FORCES AND DISPLACEMENTS PRESCRIBED IN ASCE7-05, SECTION 13.3 AS DEFINED IN ASCE7-05 SECTION 13.6.8, 13.6.7 AND 2013 CBC SECTIONS 1615A.1.20, 1615A.1.21 AND 1615A.1.22. BRACING AND ATTACHMENT TO THE STRUCTURE SHALL BE DETAILED ON APPROVED DRAWINGS OR THEY SHALL COMPLY WITH ONE OF THE OSHPD PRE-APPROVALS (OPA#) AS MODIFIED TO SATISFY ANCHORAGE REQUIREMENTS OF ACI 318, APPENDIX D.	D A6.01 B INTERIOR ELEVATIONS Detail information Sheet number / elevation
COPIES OF THE MANUAL SHALL BE AVAILABLE ON THE JOBSITE PRIOR TO THE START OF HANGING AND BRACING OF THE PIPE, DUCTWORK AND ELECTRICAL DISTRIBUTION SYSTEMS. THE STRUCTURAL ENGINEER OF RECORD SHALL VERIFY ADEQUACY OF THE STRUCTURE TO SUPPORT THE HANGER AND BRACE LOADS.	C <u>REVISION</u> AAddendum letterSupplemental instructionrevision cloud
	WORK POINT Target
	<u>MATCH LINE</u> Target
	1 ARCHITECTURAL WALL PANEL TYPE SYMBOL 1

ELEVATION TAG

SOLANO COMMUNITY COLLEGE DISTRICT 4000 Suisun Valley Road, Fairfield, California 94534 (T) 707.864.7000, www.solano.edu

LOUISE WILBOURN YARBROUGH **ICULTURE & PLANT SCIENCE INSTITUTE** AT

SOLANO COMMUNITY COLLEGE FAIRFIELD CAMPUS

4000 Suisun Valley Road, Fairfield, California 94534 (T) 707.864.7000, www.solano.edu

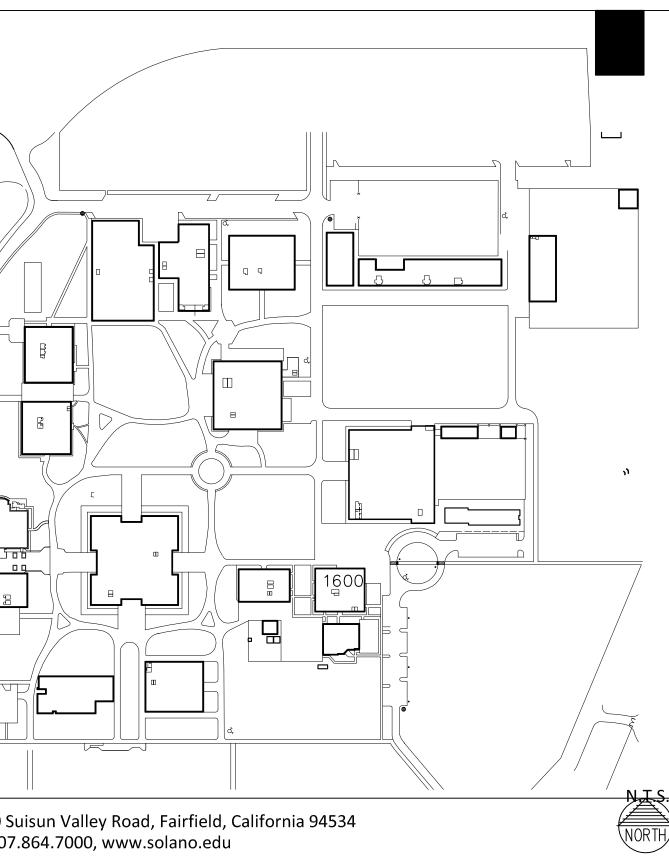
SCOPE OF WORK

ORK INCLUDES AND IS NOT LIMITED TO THE FOLLOWING:

ING, PAVING, NEW FENCING AND NEW PARKING AS SHOWN.

FARMERS MARKET STAND (SHADE STRUCTURE) LTERNATE: GREENHOUSE

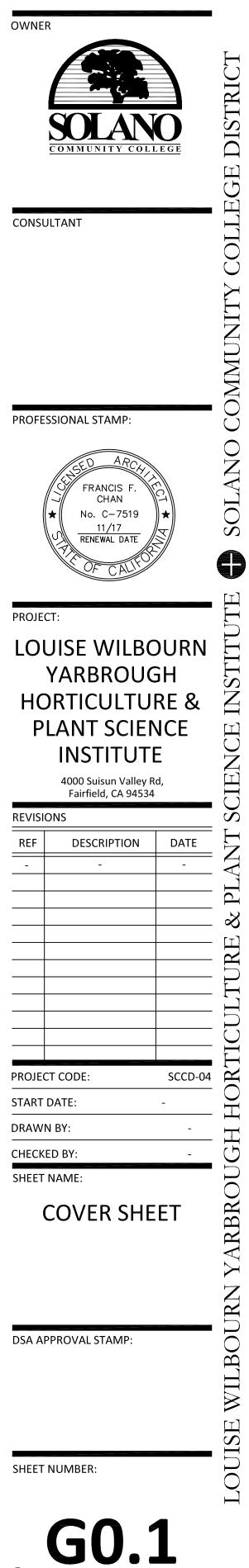
PROJECT LOCATION



ARCHITECT

MΔD ARCHITECTURE + PL/ 333 1ST STREET, SUITE C SAN FRANCISCO, CA 94105 303 POTRERO STREET, SUITE 7B SANTA CRUZ, CA 95060

TEL: 800.725.0571



GENERAL

- G0.1 COVER SHEET
- G0.2 SHEET LIST G0.3 CAMPUS SITE MAP
- CIVIL DRAWINGS
- C2 GRADING & DRAINAGE PLAN C3 UTILITY PLAN
- ARCHITECTURAL DRAWINGS A1.1 SITE PLAN - FIRE MARSHAL REVIEW
- A1.2 SITE PLAN ACCESSIBILITY PLAN
- A1.3 ENLARGED SITE PLAN
- A1.4 ENLARGED SITE PLAN
- A1.5 ENLARGED SITE PLAN
- A1.6 ENLARGED SITE PLAN
- A1.7 ENLARGED SITE PLAN A1.8 SITE DETAILS
- A1.9 SITE FENCING DETAILS
- A2.3A GREENHOUSE PLAN (BID ALTERNATE)
- A2.5A FARMERS MARKET STAND
- E0.1A ELECTRICAL SYMBOLS LIST, SCHEDULE & NOTES
- E1.1A POWER SITE PLAN E1.2A SIGNAL SITE PLAN
- E1.3A FIRE ALARM SITE PLAN
- E4.1A SIGNAL FLOOR PLANS

GREENHOUSE BY CONLEYS OR EQUAL (BID ALTERNATE)

FM-01 PLAN CONFIGURATION FM-02 DETAIL SHEET

FARMERS MARKET STAND BY AMERICANA SHELTERS WITH DSA PC 02-113840 (NO SUBSTITUTION ALLOWED) G1 DESIGN NOTES

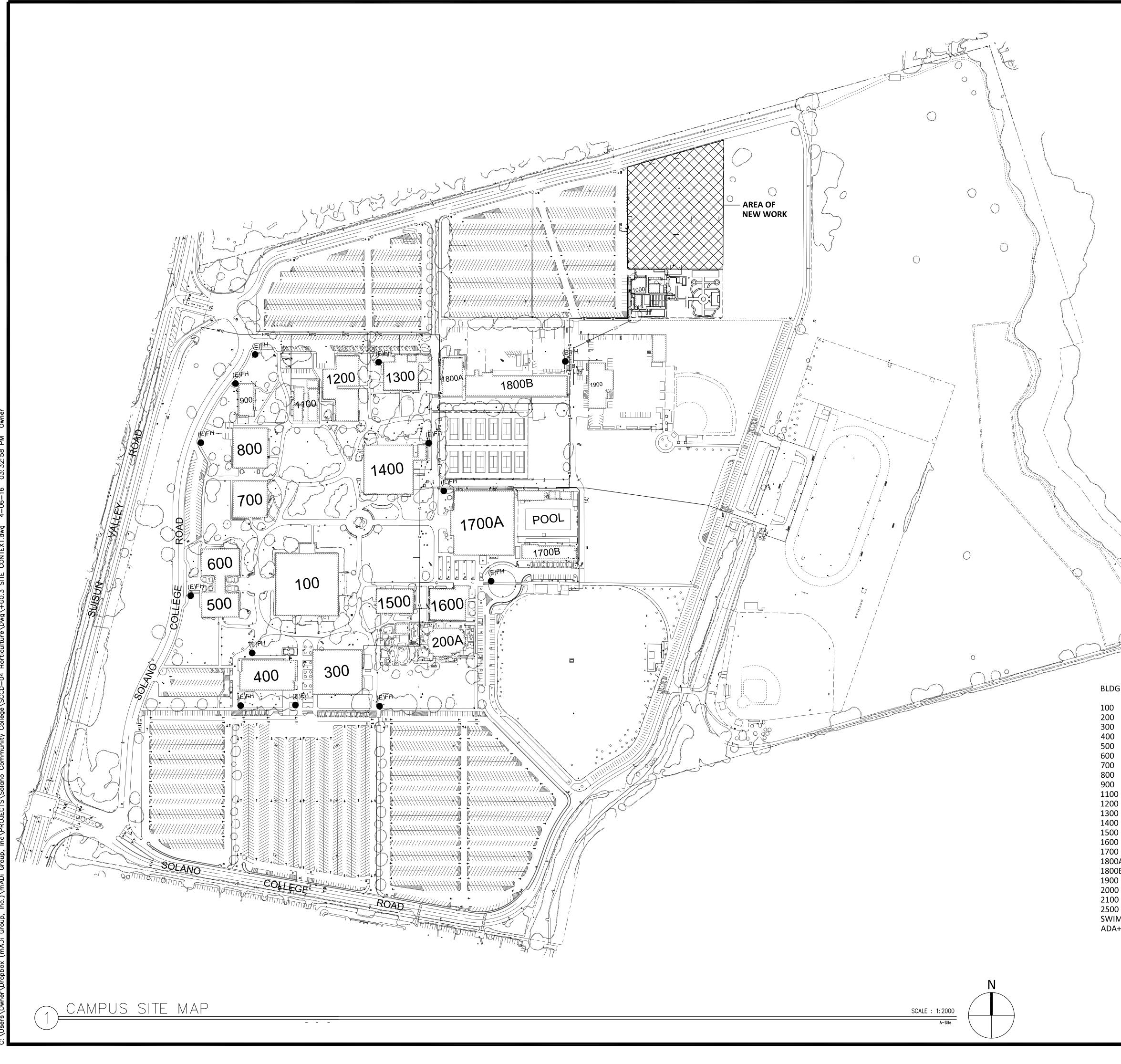
- NT30.0 DESIGN NOTES
- NT30.1 PLANS AND ELEVATIONS
- NT 30.2 SECTIONS AND DETAILS

SHEET LIST

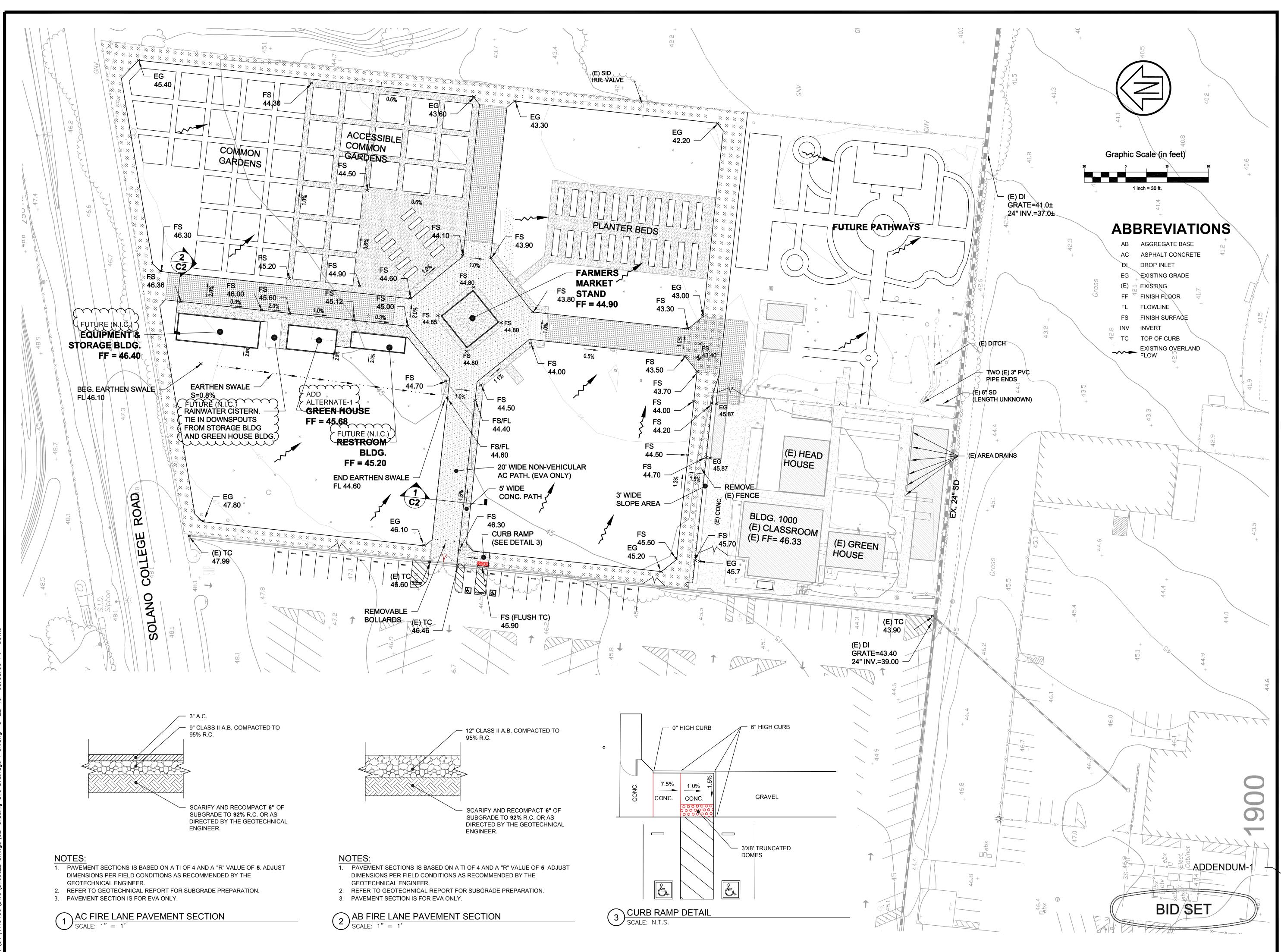
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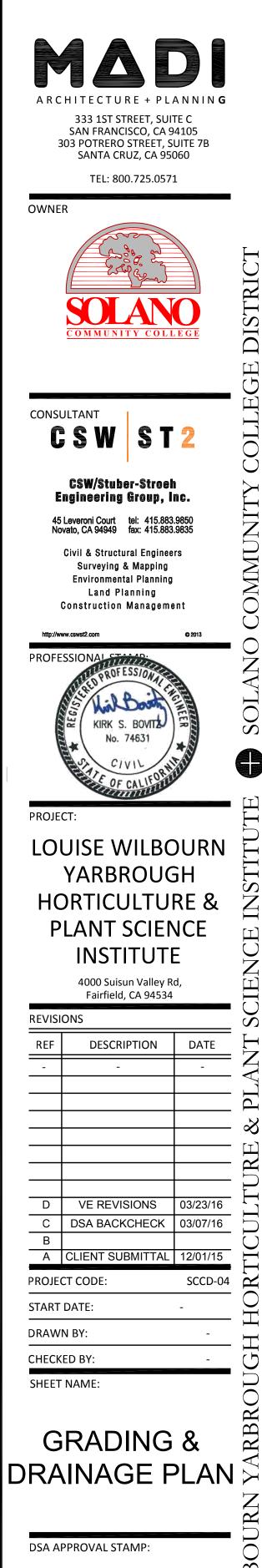
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<u>ADDENDUM-1</u>



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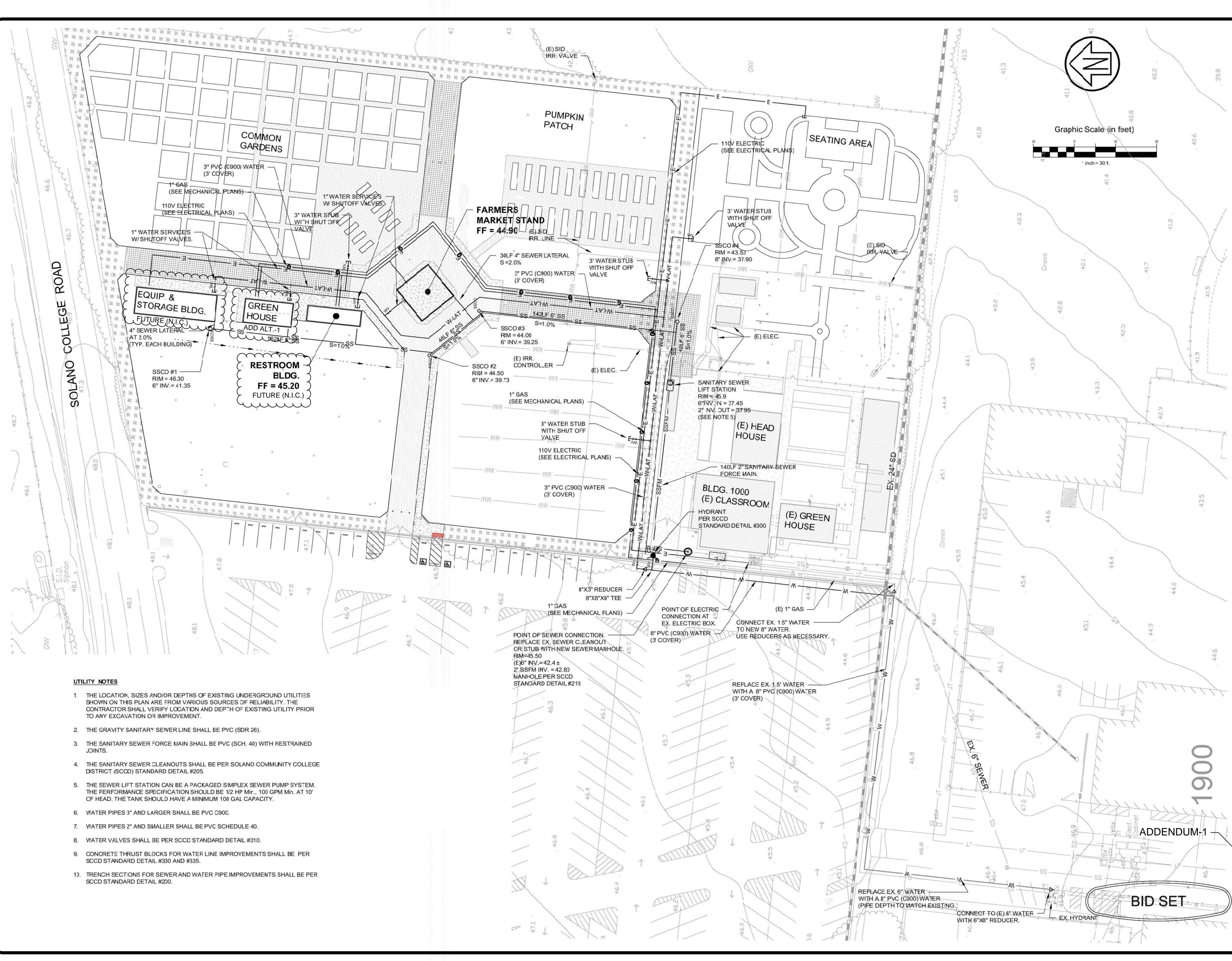




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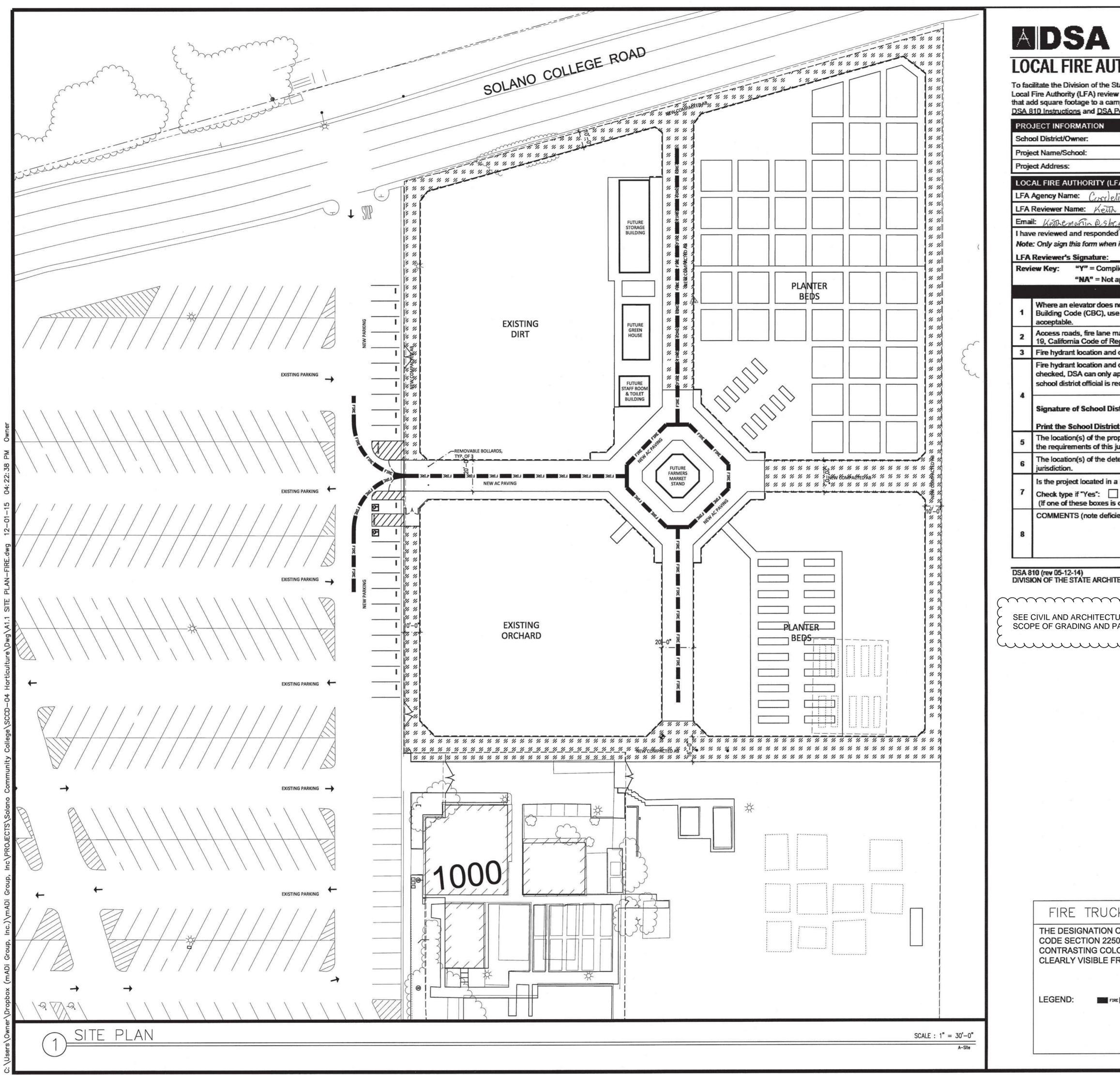
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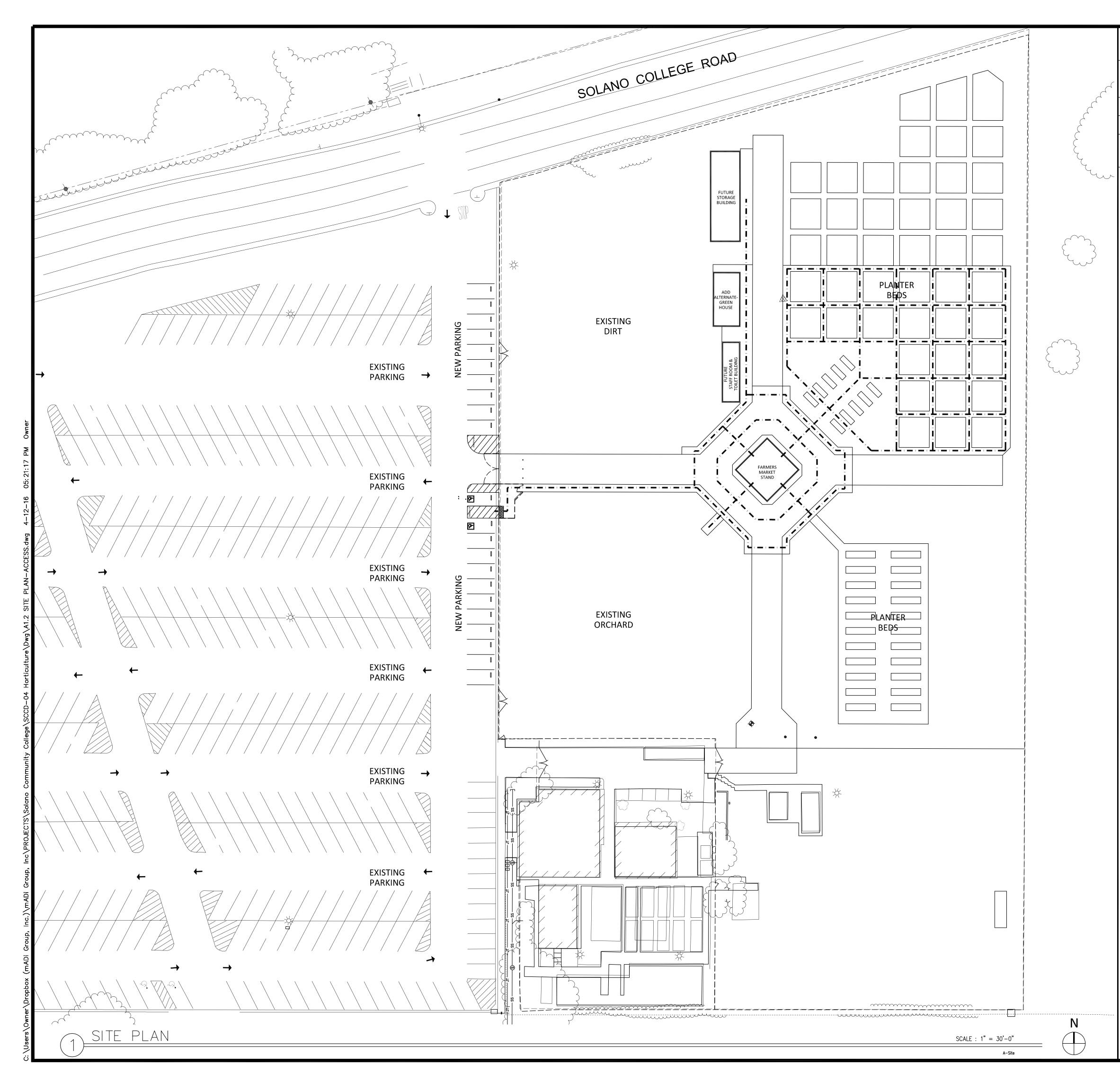


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NON-ACCESSIBLE

STALLS

PARKING LOT

1 (EXISTING) 30

ACCESSIBLE STALLS REQUIRED

1 VAN, 1 REG.

ACCESSIBLE STALLS PROVIDED ARCHITECT

1 VAN, 1 REG.

ACCESSIBLE PATH OF TRAVEL

ACCESSIBLE PATH OF TRAVEL (P.O.T.) AS INDICATED, IS A COMMON, BARRIER-FREE, FIRM AND SMOOTH ACCESS ROUTE WITHOUT ANY ABRUPT VERTICAL CHANGES EXCEEDING 1/2" BEVELED AT 1:2 MAXIMUM SLOPE. PASSING SPACES AT LEAST 60" X 60" ARE LOCATED NOT MORE THAN 200' APART. PARTS OF P.O.T.WITH CONTINUOUS GRADIENTS HAVE 60" LEVEL AREAS NOT MORE THAN 400' APART. THE CROSS-SLOPE DOES NOT EXCEED 2% AND SLOPE INTHE DIRECTION OT TRAVEL AND IS LESS THAN 5% UNLESS OTHERWISE INDICATED. (POT) SHALL BE MAINTAINED FREE OF OVERHANGING OBSTRUCTIONS TO 80" MINIMUM AND PROTRUDING OBJECTS GREATER THAN 4" PROJECTION FROM WALL AND ABOVE 27" AND LESS THAN 80".

ACCESSIBLE PATH OF TRAVEL (P.O.T.)

NOTE:

"DESIGN PROFESSIONAL IN GENERAL RESPONSIBLE CHARGE STATEMENT: THIS POT IDENTIFIED IN THESE CONSTRUCTION DOCUMENTS IS COMPLIANT WITH THE CURRENT APPLICABLE CALIFORNIA BUILDING CODE ACCESSIBILITY PROVISIONS FOR PATH OF TRAVEL REQUIREMENTS ALTERATIONS, ADDITIONS AND STRUCTURAL REPAIRS. AS PART OF THE DESIGN OF THIS PROJECT, THE POT WAS EXAMINED AND ANY ELEMENTS, COMPONENTS OR PORTIONS OF THE POT THAT WERE DETERMINED TO BE NONCOMPLIANT 1) HAVE INCLUDED WITHIN THE SCOPE OF THIS PROJECT'S WORK THROUGH DETAILS, DRAWINGS AND SPECIFICATIONS INCORPORATED INTO THESE CONSTRUCTION DOCUMENTS. ANY NONCOMPLIANT ELEMENTS, COMPONENTS OR PORTIONS OF THE POT THAT WILL NOT BE CORRECTED BY THE THIS PROJECT BASED ON VALUATION THRESHOLD LIMITATIONS OR A FINDING OF UNREASONABLE HARDSHIP ARE SO INDICATED IN THESE CONSTRUCTION DOCUMENTS.

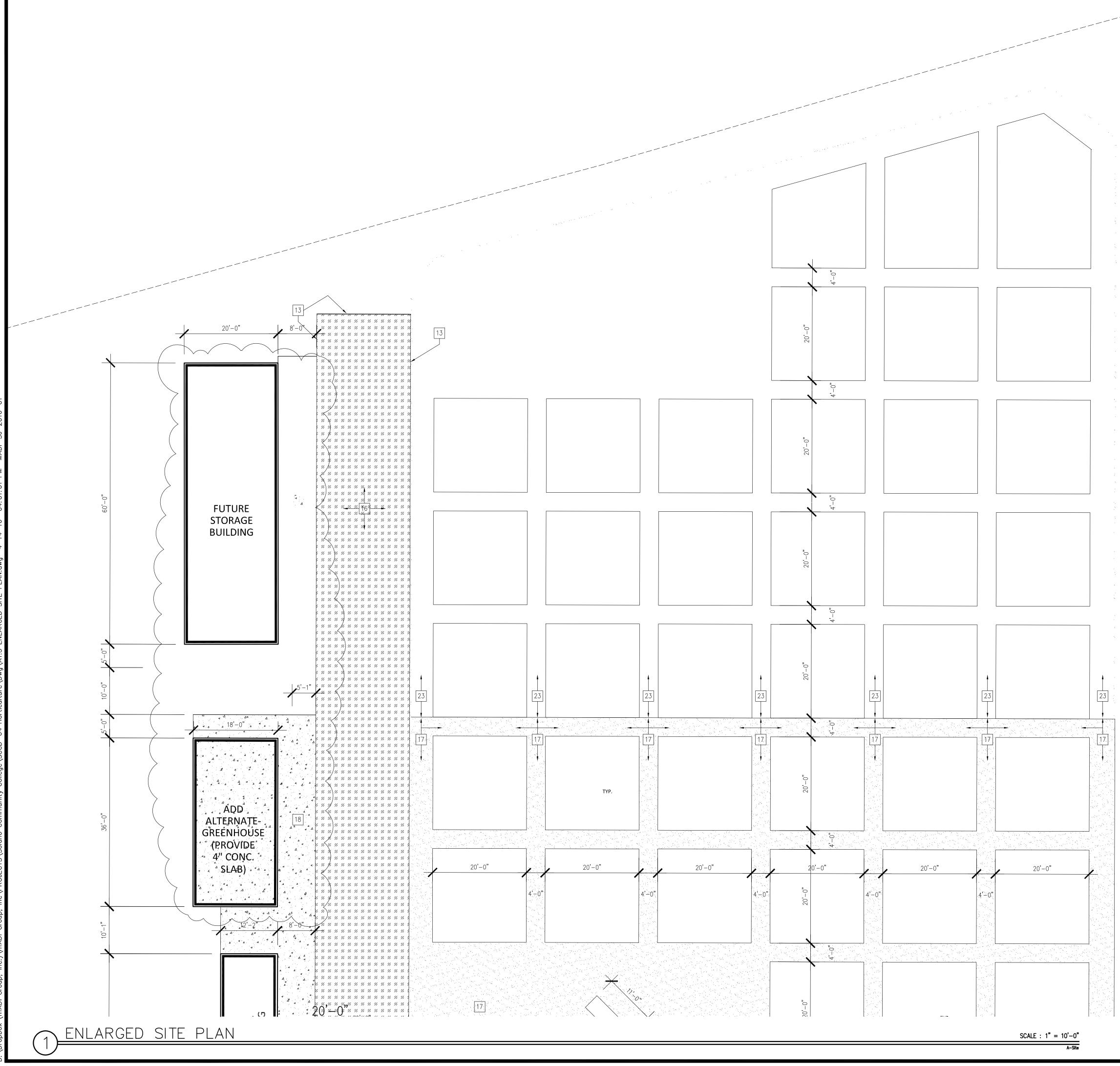
DURING CONSTRUCTION, IF POT ITEMS WITHIN THE SCOPE OF THE PROJECT REPRESENTED AS CODE COMPLIANT ARE FOUND TO BE NONCONFORMING BEYOND REASONABLE CONSTRUCTION TOLERANCES, THEY SHALL BE BROUGHT INTO COMPLIANCE WITH THE CBC AS A PART OF THIS PROJECT BY MEANS OF CONSTRUCTION CHANGE DOCUMENT."

A R C H I T E C T U R E + P L A N N I N G 333 1ST STREET, SUITE C SAN FRANCISCO, CA 94105 303 POTRERO STREET, SUITE 7B SANTA CRUZ, CA 95060 TEL: 800.725.0571 OWNER	
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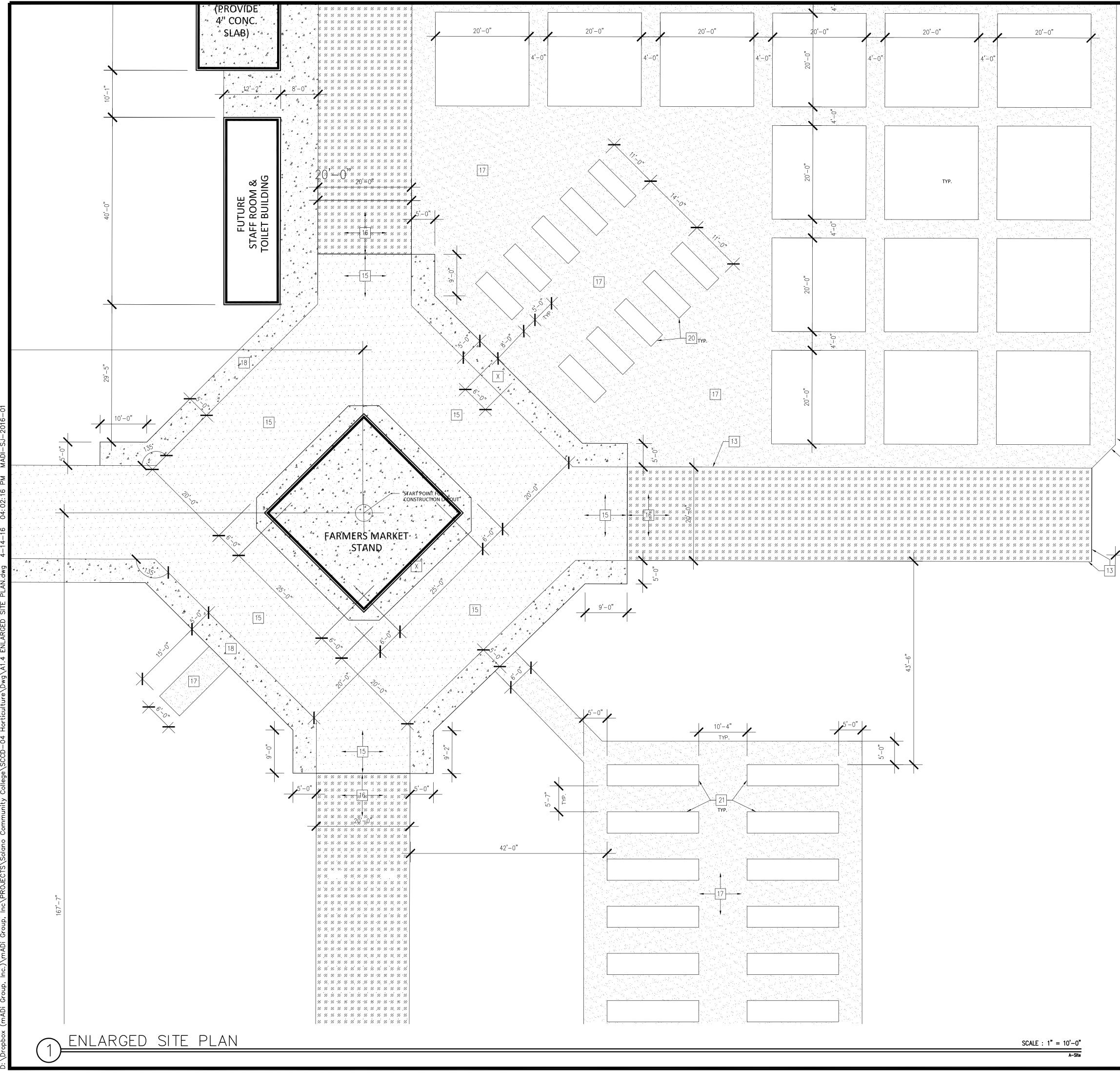
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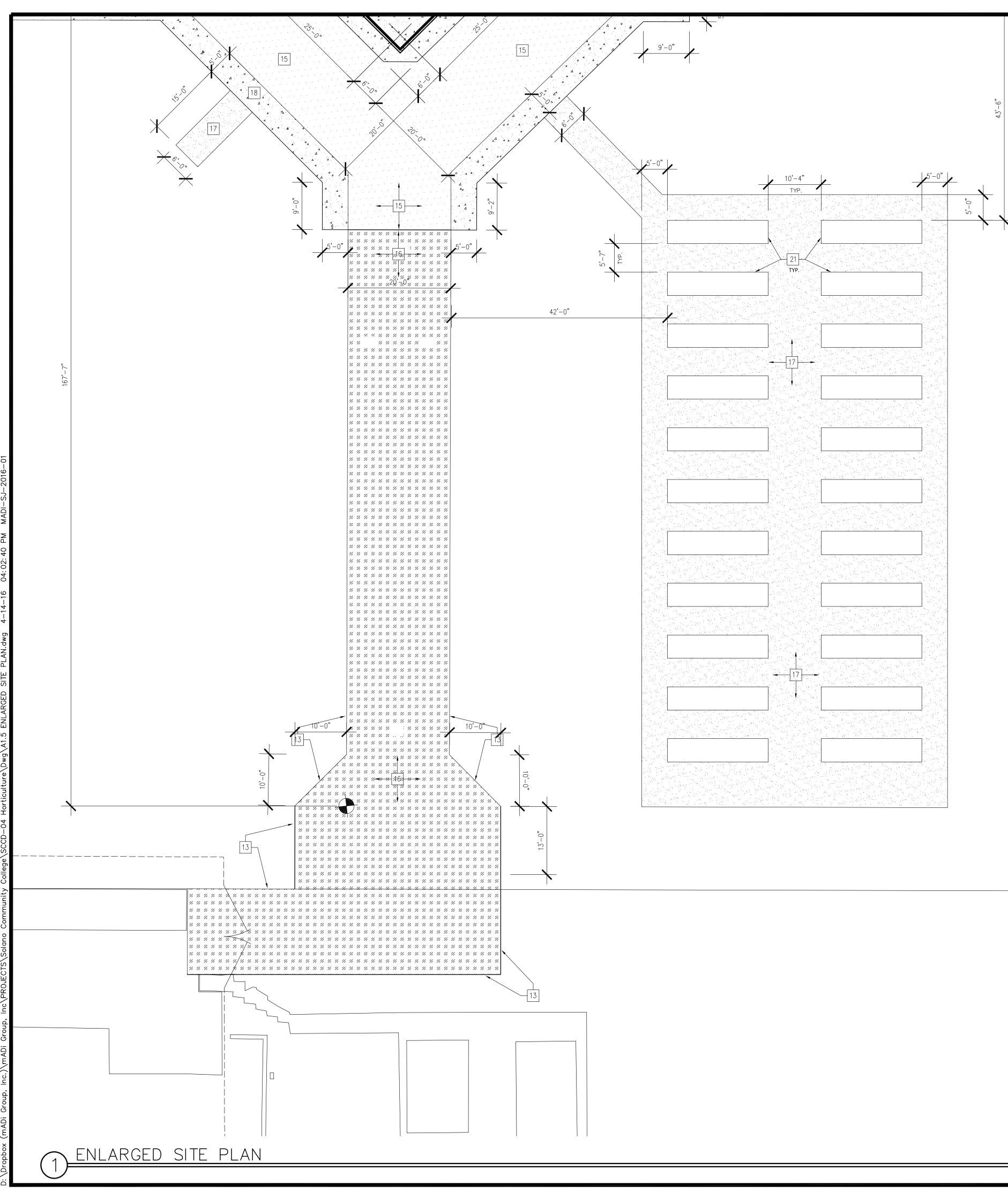
<u>ADDENDUM-1</u>



7	LEGEND	ARCHITECT
	1 DEMOLISH EXISTING FENCE AND/OR GATE	
	 2 EXISTING FENCE TO REMAIN 3 (N) 20'-0" WIDE X 6'-0" HIGH SWING GATE; SEE 6B/A1.9 	MΔDΙ
	(N) DETECTABLE WARNING STRIPS; SEE 7&8/A1.8	A R C H I T E C T U R E + P L A N N I N G 333 1ST STREET, SUITE C SAN FRANCISCO, CA 94105
	 5 (N) 3'-0" WIDE X 6'-0" HIGH SWING GATE; SEE 6A/A1.9 6 (N) ACCESSIBLE PARKING; SEE 1/A1.8 	303 POTRERO STREET, SUITE 7B SANTA CRUZ, CA 95060
	7 (N) PARKING STRIPING	TEL: 800.725.0571
	8 (N) WHEELSTOP; SEE 9/A1.8	OWNER
	 9 (N) REMOVABLE BOLLARDS; SEE 4/A1.8 10 (N) SIGNAGE; SEE 10/A1.8 	
	11 (N) SIGNAGE; SEE 11/A1.8	SOLANO COMMUNITY COLLEGE
	12 (N) SIGNAGE; SEE 12/A1.8 13 (N) REDWOOD HEADER EDGE; SEE 5/A1.8 14 (N) 6'-0" HIGH CHAINLINK FENCE	SOLANO COMMUNITY COLLEGE
	15 (N) AC PAVING	CONSULTANT
	16 (N) AB PAVING	
	18 (N) CONCRETE PAVING	ΥC
	19 NOT USED	
	20 (N) 3'-6"X11'-0" PLANTERS	
	21 (N) 4'-6"X20'-0" PLANTERS	
	22 (N) 4'-0" HIGH X 5'-0" SLIDING GATE; SEE 1/A1.9. PROVIDE SIGN STATING "ENTRY CONTROLLED AND RESTRICTED BY SECURITY PERSONNEL" PER CBC 11B-404.1 EXCEPTION 1.	PROFESSIONAL STAMP:
	23 (E) DIRT	FRANCIS F. CHAN
	24 (N) SIGNAGE; SEE 3/A1.8	(★ No. C−7519 ★
		RENEWAL DATE
		CALIFOR CALIFOR
		PROJECT:
		YARBROUGH
		PLANT SCIENCE
		4000 Suisun Valley Rd,
		Fairfield, CA 94534
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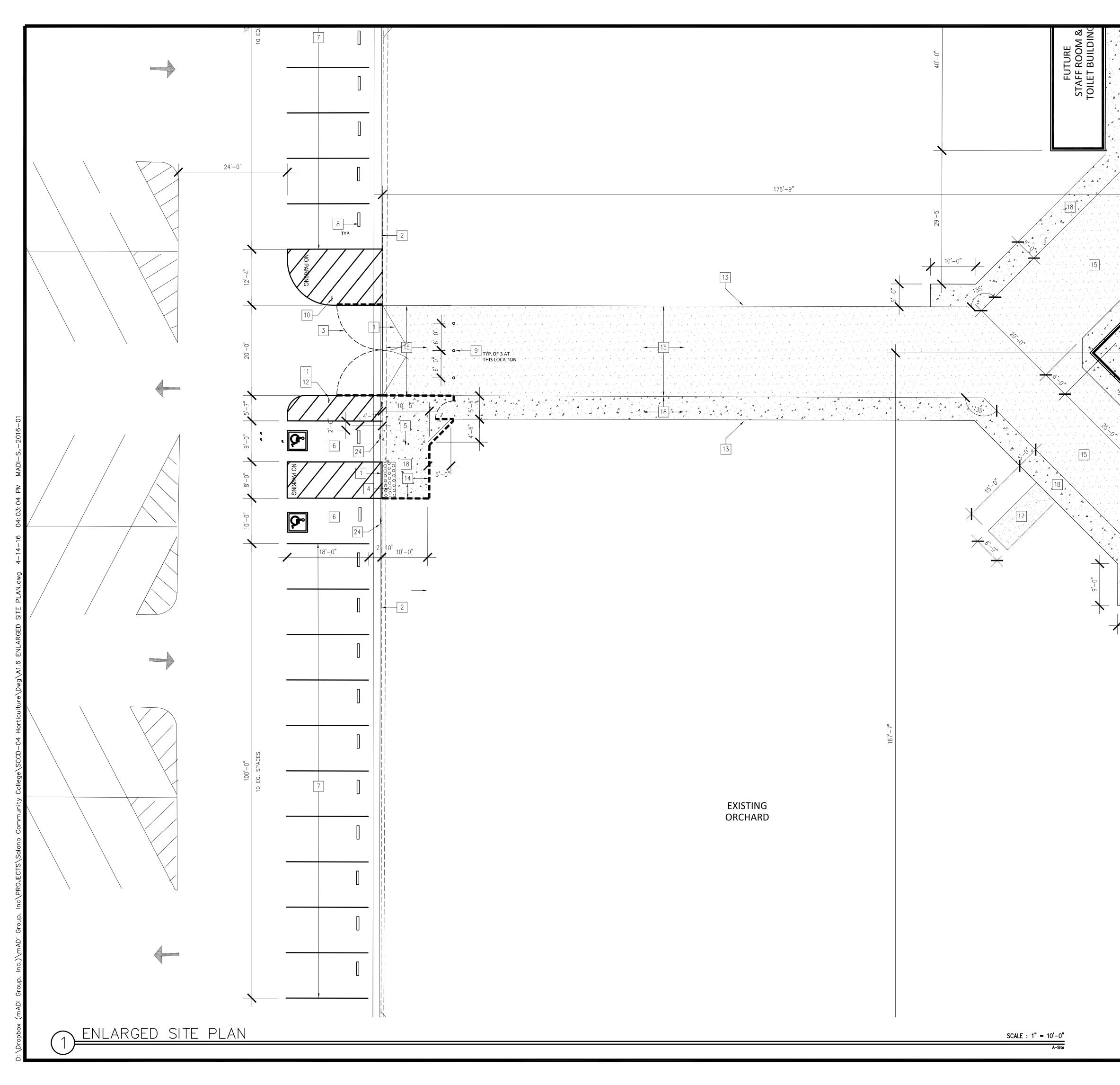


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		LEGEND		
		1 DEMOLISH EXISTING FENCE AND/OR GATE		
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		4 (N) DETECTABLE WARNING STRIPS; SEE 7&8/A1.8	A R C H I T E C T U R E + P L A N N I N G 333 1ST STREET, SUITE C	
		5 (N) 3'-0" WIDE X 6'-0" HIGH SWING GATE; SEE 6A/A1.9	SAN FRANCISCO, CA 94105 303 POTRERO STREET, SUITE 7B SANTA CRUZ, CA 95060	
		6 (N) ACCESSIBLE PARKING; SEE 1/A1.8	TEL: 800.725.0571	
 		 7 (N) PARKING STRIPING 8 (N) WHEELSTOP; SEE 9/A1.8 	OWNER	
		9 (N) REMOVABLE BOLLARDS; SEE 4/A1.8		F
		10 (N) SIGNAGE; SEE 10/A1.8		ПС
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		12 (N) SIGNAGE; SEE 12/A1.8 13 (N) REDWOOD HEADER EDGE; SEE 5/A1.8	COMMUNITY COLLEGE	DIG
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		(17 (N) DG PAVING.		Ŭ
		18 (N) CONCRETE PAVING		L I
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		20 (N) 3'-6"X11'-0" PLANTERS		NUMMC
		22 (N) 4'-0" HIGH X 5'-0" SLIDING GATE; SEE 1/A1.9. PROVIDE SIGN		NO NO
		STATING "ENTRY CONTROLLED AND RESTRICTED BY SECURITY PERSONNEL" PER CBC 11B-404.1 EXCEPTION 1.	PROFESSIONAL STAMP:	\bigcirc
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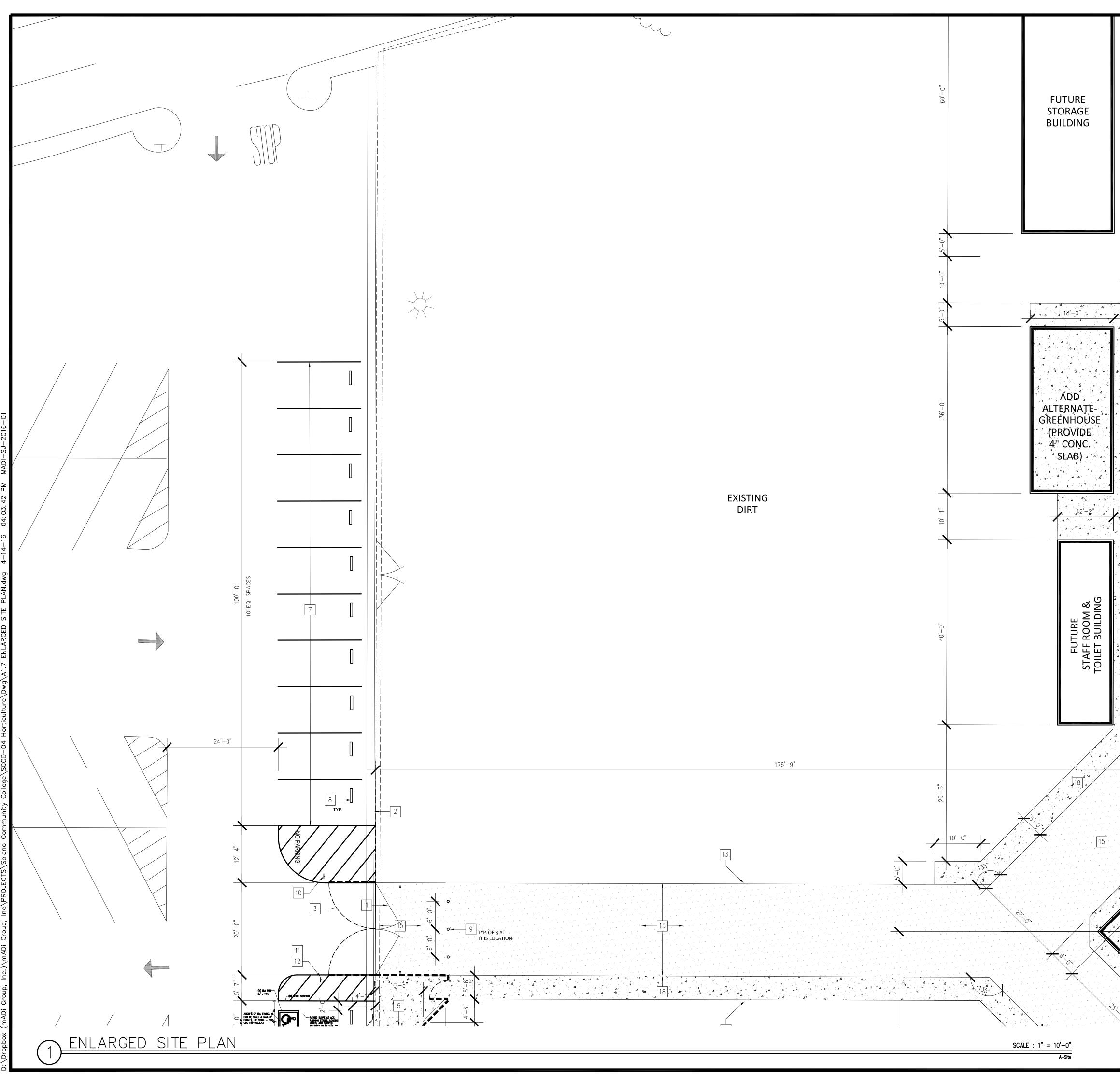


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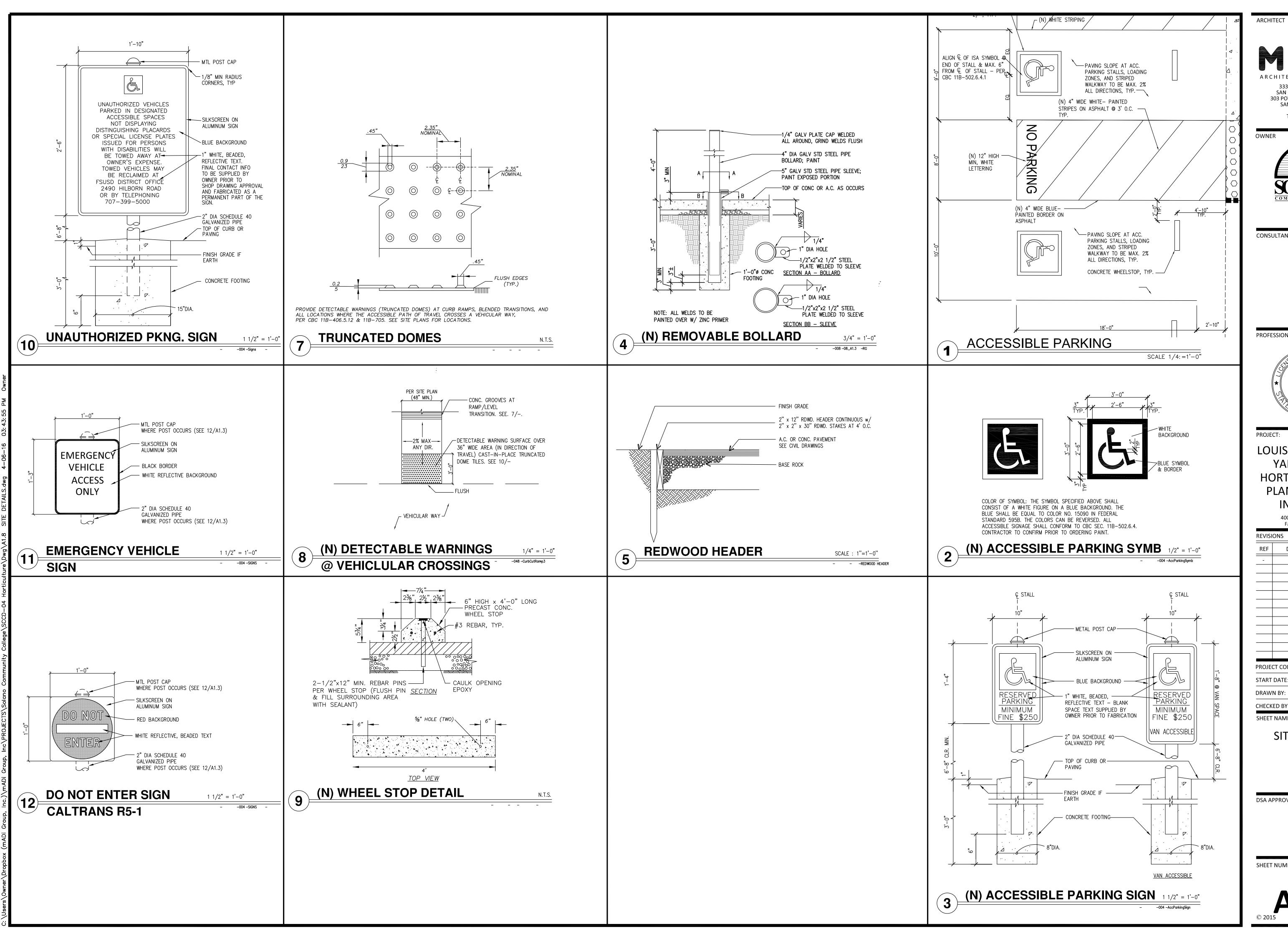
LEGEND	ARCHITECT	
1 DEMOLISH EXISTING FENCE AND/OR GATE		
2 EXISTING FENCE TO REMAIN 3 (N) 20'-0" WIDE X 6'-0" HIGH SWING GATE; SEE 6B/A1.9	MAD	
 3 (N) 20'-0" WIDE X 6'-0" HIGH SWING GATE; SEE 6B/A1.9 4 (N) DETECTABLE WARNING STRIPS; SEE 7&8/A1.8 	A R C H I T E C T U R E + P L A N N I N 333 1ST STREET, SUITE C	G
5 (N) 3'-0" WIDE X 6'-0" HIGH SWING GATE; SEE 6A/A1.9	SAN FRANCISCO, CA 94105 303 POTRERO STREET, SUITE 7B	
6 (N) ACCESSIBLE PARKING; SEE 1/A1.8	SANTA CRUZ, CA 95060 TEL: 800.725.0571	
7 (N) PARKING STRIPING	OWNER	
8 (N) WHEELSTOP; SEE 9/A1.8 9 (N) REMOVABLE BOLLARDS; SEE 4/A1.8	OWNER	
10 (N) SIGNAGE; SEE 10/A1.8		
11 (N) SIGNAGE; SEE 11/A1.8		
12 (N) SIGNAGE; SEE 12/A1.8 13 (N) REDWOOD HEADER EDGE; SEE 5/A1.8 14 (N) 6'-0" HIGH CHAINLINK FENCE	COMMUNITY COLLEGE	
15 (N) AC PAVING		
16 (N) AB PAVING	CONSULTANT	
(17 (N) DG PAVING.		
18 (N) CONCRETE PAVING		
19 NOT USED		
20 (N) 3'-6"X11'-0" PLANTERS		
21 (N) 4'-6"X20'-0" PLANTERS		
(N) 4'-0" HIGH X 5'-0" SLIDING GATE; SEE 1/A1.9. PROVIDE SIGN STATING "ENTRY CONTROLLED AND RESTRICTED BY SECURITY DEDSONNEL" DEP CPC 11B 404 1 EXCEPTION 1	PROFESSIONAL STAMP:	
PERSONNEL" PER CBC 11B-404.1 EXCEPTION 1.	CED ARCL	
24 (N) SIGNAGE; SEE 3/A1.8	FRANCIS F. CHAN	
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	4000 Suisun Valley Rd,	
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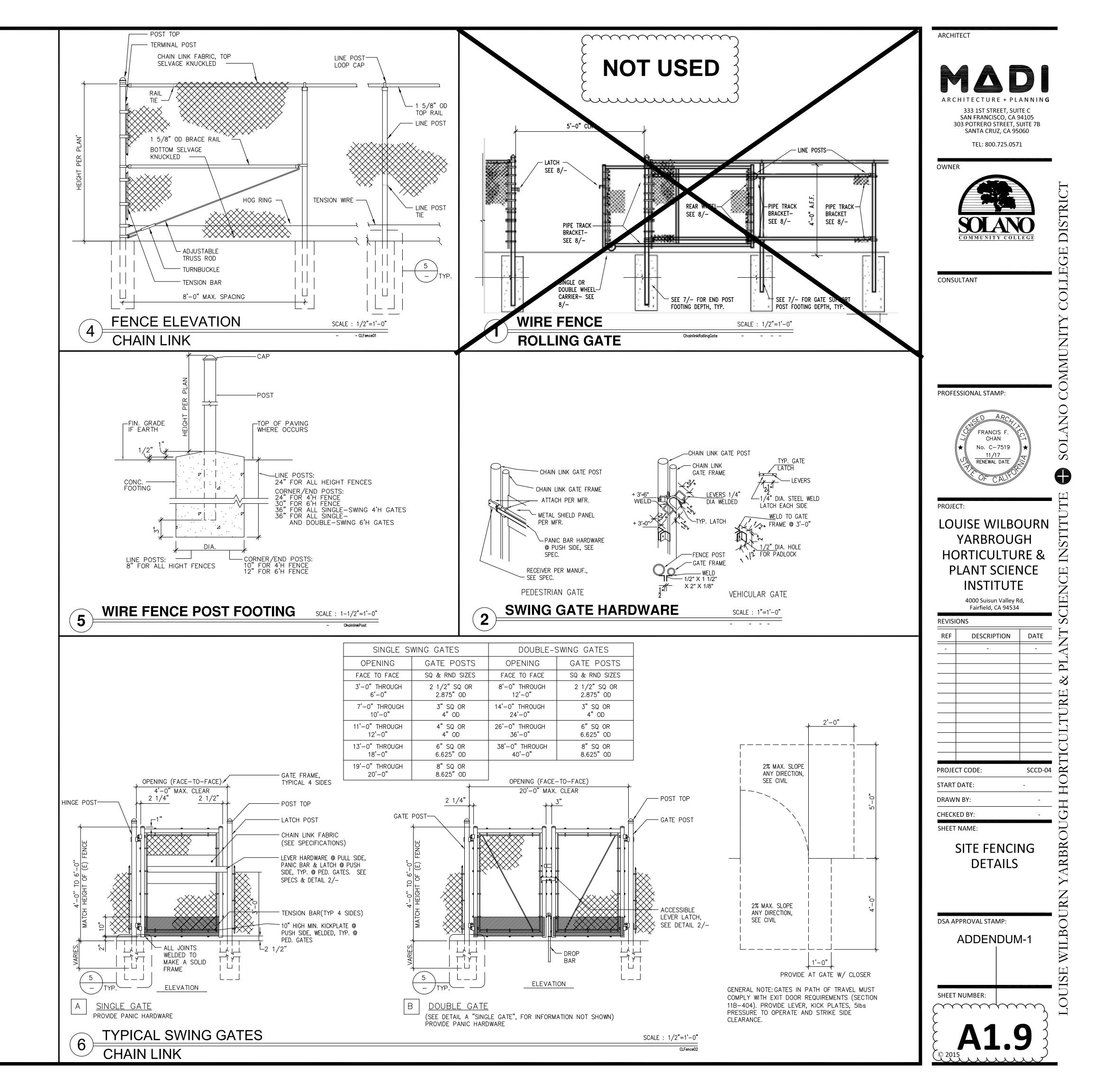
▲ ▲ ₩ <u>₩₩₩₩₩₩₩₩₩₩</u>	LEGEND	ARCHITECT
	 DEMOLISH EXISTING FENCE AND/OR GATE EXISTING FENCE TO REMAIN (N) 20'-0" WIDE X 6'-0" HIGH SWING GATE; SEE 6B/A1.9 	MΔDΙ
	(N) DETECTABLE WARNING STRIPS; SEE 7&8/A1.8	A R C H I T E C T U R E + P L A N N I N G 333 1ST STREET, SUITE C SAN FRANCISCO, CA 94105
	5(N) 3'-0" WIDE X 6'-0" HIGH SWING GATE; SEE 6A/A1.96(N) ACCESSIBLE PARKING; SEE 1/A1.8	303 POTRERO STREET, SUITE 7B SANTA CRUZ, CA 95060 TEL: 800.725.0571
	 7 (N) PARKING STRIPING 8 (N) WHEELSTOP; SEE 9/A1.8 	OWNER
	9 (N) REMOVABLE BOLLARDS; SEE 4/A1.8	
	10 (N) SIGNAGE; SEE 10/A1.8 11 (N) SIGNAGE; SEE 11/A1.8	
	12 (N) SIGNAGE; SEE 12/A1.8	SOLANO
	(N) REDWOOD HEADER EDGE; SEE 5/A1.8 [14] (N) 6'-0" HIGH CHAINLINK FENCE	COMMUNITY COLLEGE
	14 (N) 6'-0" HIGH CHAINLINK FENCE 15 (N) AC PAVING	
	16 (N) AB PAVING (17) (N) DG PAVING.	CONSULTANT
	18 (N) CONCRETE PAVING	K K
	19 NOT USED	
	20 (N) 3'-6"X11'-0" PLANTERS	MU
FARMERS M	[22] (N) 4'-0" HIGH X 5'-0" SLIDING GATE; SEE 1/A1.9. PROVIDE SIGN	OMM
	PERSONNEL" PER CBC 11B-404.1 EXCEPTION 1.	PROFESSIONAL STAMP:
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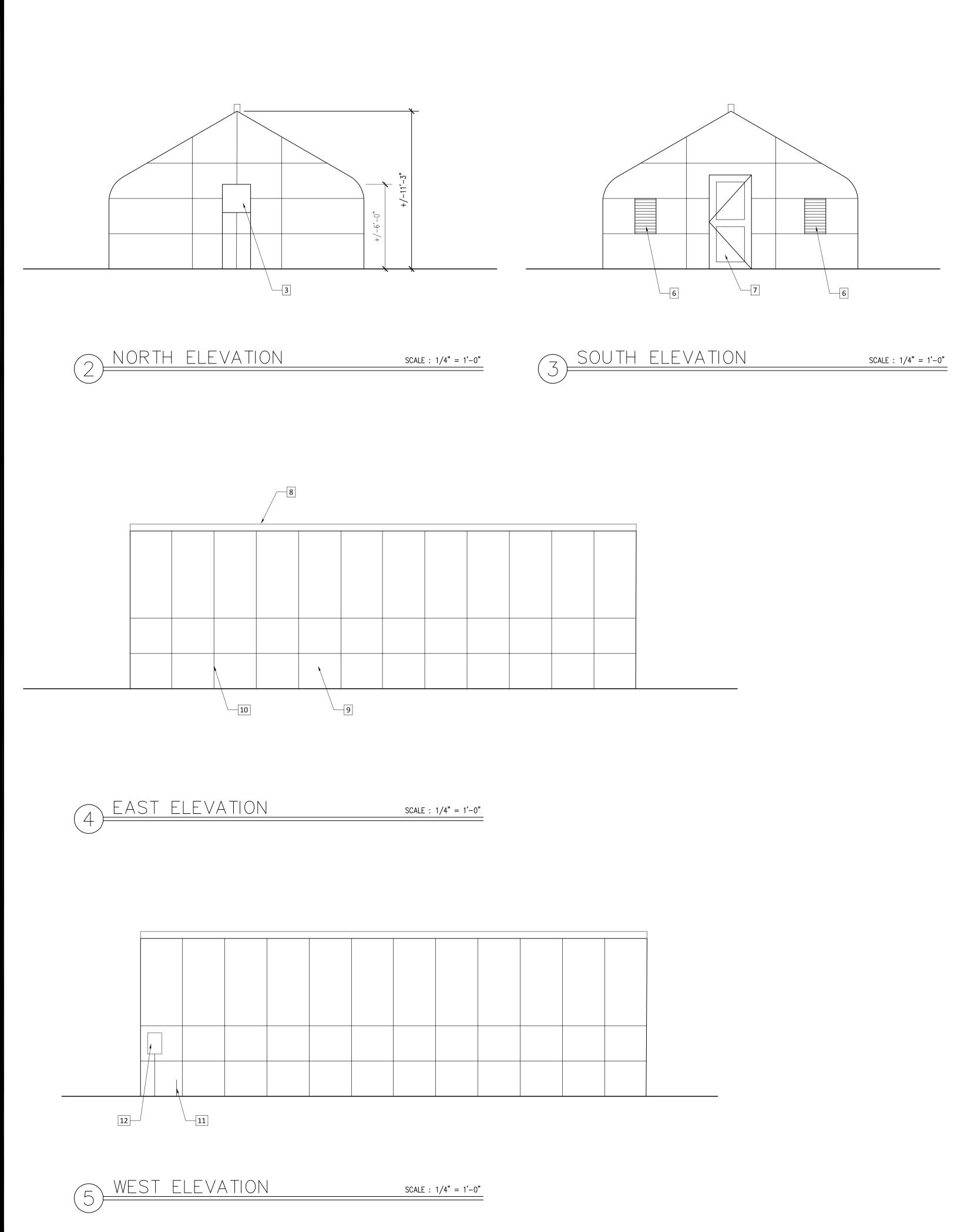


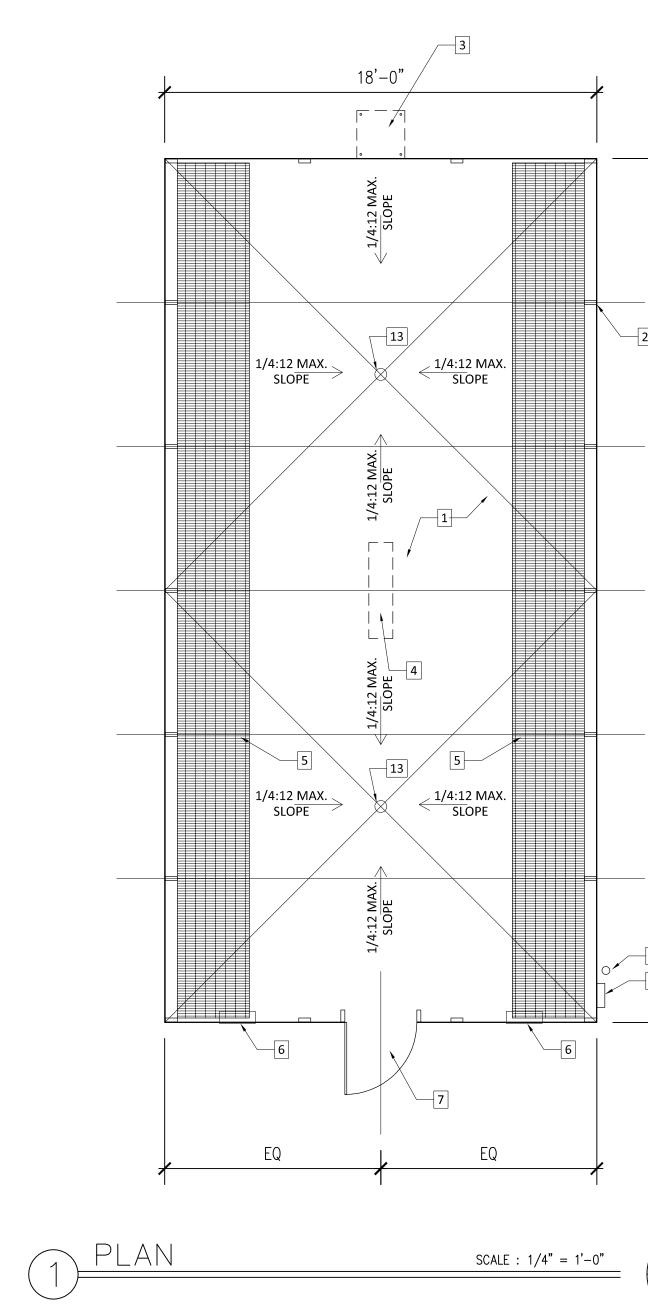
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	6	: 1, 1, : 1, 1,	- 11, 11, - 11, 11,	· // // · // // · // //	9 (N) REMOVABLE BOLLARDS; SEE 4/A1.8	
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Δ Δ.	1, 1, 1, 1, 1, 1,	:	", ", ", ",	\$ % % \$ % % \$ % %	24 (N) SIGNAGE; SEE 3/A1.8	$\begin{array}{c} FRANCIS F. \\ FRANCIS F. \\ FRANCIS F. \\ CHAN \\ No. C-7519 \\ 11/17 \\ No. C-7519 \\ No. C-7510 \\ $
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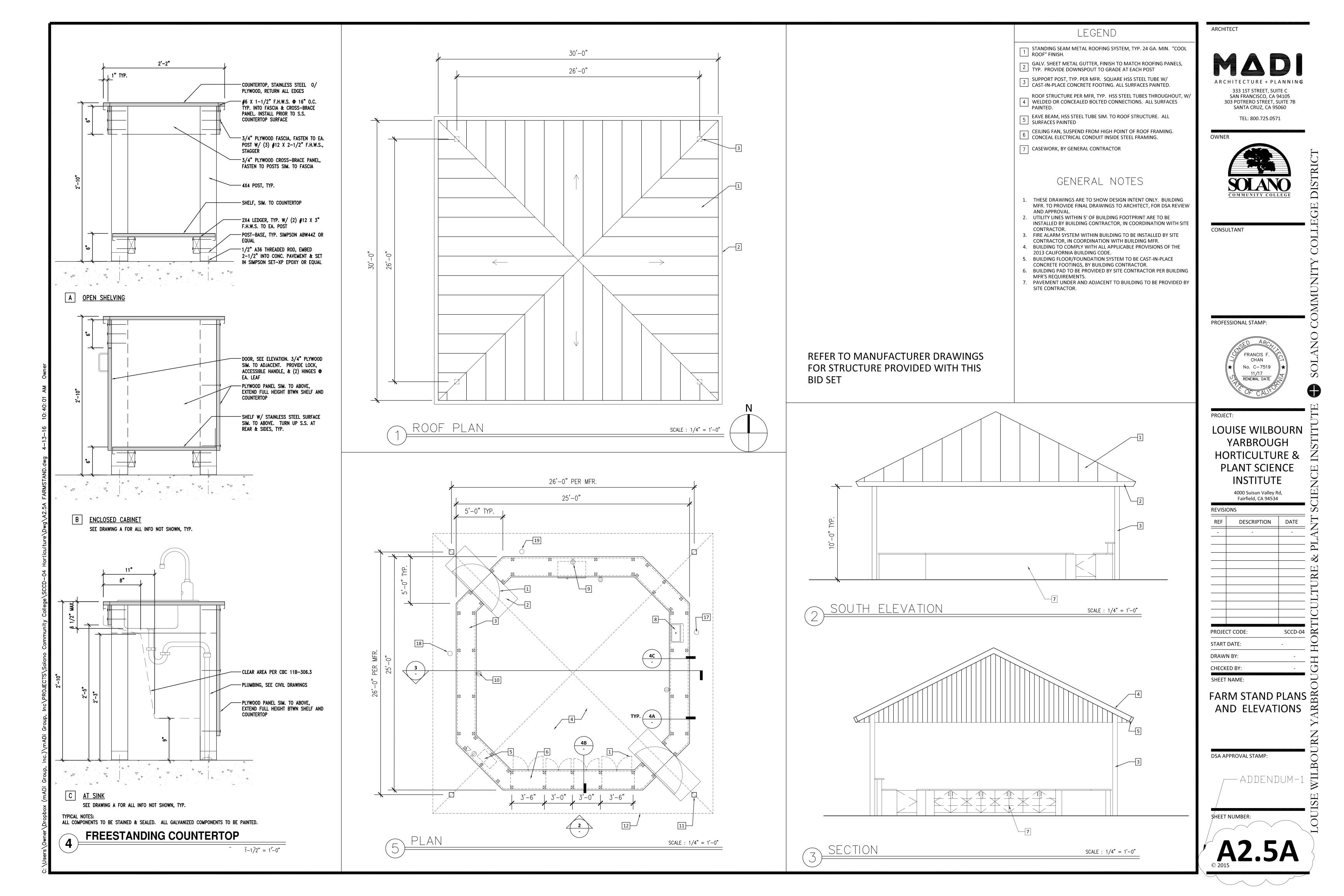








LEGEND	ARCHITECT
 4" THICK CONCRETE FLOOR SLAB & FOOTINGS. SLOPE TO DRAIN, 1/4:12 MAX. GALVANIZED STEEL BLDG. FRAME, TYP. ROLL-FORMED. ALL FASTENER HOLES PRE-DRILLED PRIOR TO GALVANIZATION. EVAPORATIVE COOLER, 3/4 HP, W/ THRU-WALL LOUVERED VENT & SUPPORT LEGS BY MFR. 60,000 BTU GAS HEATER, ABOVE. HANGER HARDWARE BY MFR. 3'-0" WIDE, FULL-LENGTH BUILT-IN METAL SHELF W/ EXPANDED METAL SURFACE, TYP. LOUVERED THRU-WALL VENT W/ 12" DIA. AIRFLOW FAN, TYP. 3'-0" X 6'-8" DOOR W/ GLAZED LITES & LOCKING ACCESSIBLE LEVER HARDWARE MOTORIZED RIDGE VENT ASSEMBLY, FULL LENGTH OF BLDG. GLAZED WALL PANELS, TYP. 6mm DUAL-WALL POLYCARB PANELS, UV CONTROL @ EXTERIOR, CONDENSATION CONTROL @ INTERIOR. ANOD. ALUMINUM EXTRUSIONS @ ALL PANEL JOINTS, TYP. ANPROX. LOCATION OF NEW GAS CONNECTION, SEE SITEWORK DRAWINGS APPROX. LOCATION OF NEW ELECTRICAL CONNECTION & PANEL, SEE SITEWORK DRAWINGS NEW AREA DRAIN BY SITE CONTRACTOR, CONNECT TO SITE SEWER LINE, SEE SITEWORK DRAWINGS 	<section-header><section-header><section-header><text><text><text><text><text></text></text></text></text></text></section-header></section-header></section-header>
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GENERAL NOTES:

- MOUNTING HEIGHT IS TO THE CENTER OF EQUIPMENT, U.O.N. MOUNTING HEIGHTS OF SUSPENDED LIGHT FIXTURES ARE TO THE BOTTOM OF THE FIXTURE. U.O.N.
- RECEPTACLES AND DEVICES INSTALLED ABOVE COUNTER SHALL HAVE THE BOTTOM OF COVER PLATE AT APPROX 2-INCHES ABOVE COUNTER OR BACKSPLASH.
- 3. CAP ALL EMPTY CONDUITS FOR FUTURE USE WATERTIGHT WITH MANUFACTURERS END CAP, WITH PULL STRING ATTACHED.
- 4. SEAL ALL EXTERIOR WALL PENETRATIONS WATERTIGHT WITH SILICONE GROUT.
- 5. SEAL ALL WALL AND CEILING PENETRATIONS WITH GROUT. WHERE CONDUITS PENETRATE FIRE RATED BARRIERS, SEAL PENETRATIONS WITH FIRE RATED COMPOUND TO MATCH OR EXCEED BARRIER RATING.
- 6. PENETRATIONS OF FIRE RATED ASSEMBLIES SHALL BE SEALED AS REQUIRED BY CBC.
- 1. ALL CONDUITS AND BOXES ON THE EXTERIOR SHALL BE PAINTED TO MATCH THE ADJACENT FINISH.
- 8. WHERE FIRE RATED CONSTRUCTION IS REQUIRED (REFER TO ARCHITECTURAL DRAWINGS), DO NOT LOCATE ELECTRICAL OUTLET BOXES BACK-TO-BACK. PROVIDE MINIMUM 24" HORIZONTAL SEPARATION BETWEEN OUTLET BOXES PER CBC.
- 9. FIRE STOPPING SHALL BE PROVIDED WHERE PENETRATING ITEMS PASS ENTIRELY THROUGH BOTH PENETRATIVE MEMBRANES OF BEARING WALLS REQUIRED TO HAVE A FIRE-RESISTIVE RATING AND WALLS REQUIRING PROTECTED OPENINGS. FIRE STOPPING SHALL ALSO BE PROVIDED AT PENETRATIONS OF FIRE RESISTIVE FLOORS AND FLOORS WHICH ARE PART OF A CEILING-FLOOR ASSEMBLY, FIRE-STOPPING SHALL HAVE AN "F" AND/OR "T" RATING AS DETERMINED BY TESTS CONDUCTED IN ACCORDANCE WITH CBC STD. 43-6.
- 10. JUNCTION BOXES, CABINETS, EQUIPMENT ENCLOSURES, SWITCHES, PANELS, ETC. INSTALLED OUTDOORS, OR IN WET OR DAMP LOCATIONS, SHALL BE RATED NEMA-3R FOR OUTDOOR ENVIRONMENTS. PROVIDE MINIMUM 1/4" AIR GAP BETWEEN ENCLOSURE AND WALL SURFACE. PROVIDE GALVANIZED METAL CHANNELS FOR MOUNTING ENCLOSURE ONTO WALL AS REQUIRED.
- 11. ALL BOXES FOR LIGHT SWITCHES SHALL HAVE CIRCUIT ID HANDWRITTEN (WITH PERMANENT FELT PEN) ON THE BACK INSIDE OF THE BOX.
- 12. ALL RECEPTACLES SHALL HAVE CIRCUIT ID ON THE COVERPLATE. USE TYPEWRITTEN "CLEAR TAPE". CLEAN SURFACE BEFORE ADHESIVE TAPE IS APPLIED. SAMPLE, "HA-11".
- 13. ALL WIRING SHALL BE IN CONDUIT, ALL CIRCUITS SHALL BE CONCEALED EXCEPT THAT ON EXISTING SURFACE AND IN DRY LOCATIONS WHERE NECESSARY AND ACCEPTABLE TO THE ARCHITECT, SURFACE METAL RACEWAY (SMR) CAN BE USED, WIREMOLD OR EQUAL. 1/2" CONDUIT WITH LESS THAN 5#12 WIRES SHALL CORRESPOND TO A V200 RACEWAY, OTHERWISE USE V500; 3/4" CONDUIT SHALL CORRESPOND TO A V100; I" CONDUIT SHALL CORRESPOND TO A V2000; 1-1/4" CONDUIT SHALL CORRESPOND TO A V2400BC. SMR SHALL BE IVORY COLOR AND SHALL BE SECURED TO SURFACES WITH 2 HOLE STRAPS. PROVIDE ALL FITTINGS, ADAPTERS, COUPLINGS, BOXES, ETC. AS REQUIRED FOR A COMPLETE SYSTEM. PROVIDE MATCHING SURFACE OUTLET BOX. PAINT TO MATCH ADJACENT FINISH.
- 14. DEVICE AND EQUIPMENT HEIGHTS SHALL BE COORDINATED WITH ARCHITECTURAL PLANS AND ELEVATIONS. CONFLICTS SHALL BE ADDRESSED TO THE ARCHITECT PRIOR TO ROUGH-IN.
- 15. COORDINATE EXACT LOCATION OF EXTERIOR WALL LIGHT FIXTURES, SPEAKERS, ETC. WITH ARCHITECTURAL ELEVATIONS.
- 16. ELECTRICAL CIRCUITS TO AC UNITS SHALL COME UP INSIDE OF AC CURBS, UNLESS THE AC UNIT DOES NOT ALLOW THIS.
- 17. IN CERTAIN ROOMS, CIRCUITING AND DEVICES/EQUIPMENT IN ONE ROOM ARE INDICATED TO BE SIMILAR TO ANOTHER ROOM'S. PROVIDE ALL SUCH CONDUIT, WIRING DEVICES, AND EQUIPMENT TO BE THE SAME AS THE OTHER ROOM INDICATED. MAKE NECESSARY MINOR ADJUSTMENTS FOR SIMILAR ROOMS THAT ARE OPPOSITE HAND, FLIP-FLOPPED, MIRRORED, OR MINOR WALL DIFFERENCES. THE FOLLOWING ITEMS ARE NOT INCLUDED IN THIS SIMILAR LAYOUT AND ARE SPECIFIC TO EACH ROOM, UNLESS SPECIFICALLY NOTED OTHERWISE.
- A. AIR CONDITIONING AND MECHANICAL EQUIPMENT CONNECTIONS. B. EQUIPMENT THAT IS N.I.E.S. BUT REQUIRE ELECTRICAL CONNECTIONS.
- C. LAYOUT OF THE CABLE SUPPORT SYSTEM (CABLE HOOKS OR CABLE TRAY)
- 18. NOT USED
- 19. FOR CONDUITS ROUTED BELOW FOOTING AT ELECTRICAL ROOMS, COORDINATE WITH STRUCTURAL DRAWINGS.

EXISTING CONDITIONS:

- DEVICES / EQUIPMENT AND CIRCUITING SHOWN AS EXISTING AND/OR EXISTING TO BE REMOVED ARE BASED ON REVIEW OF EXISTING AVAILABLE DOCUMENTS AND VISUAL FIELD VERIFICATION. SUCH INFORMATION MAY NOT BE ACCURATE. PRIOR TO DEMOLITION AND CONSTRUCTION, CONTRACTOR SHALL FIELD VERIFY EXISTING CONDITIONS TO DETERMINE ACCURACY. WHERE EXISTING CONDITIONS DO NOT REFLECT THE INFORMATION SHOWN ON THE PLANS, AND WHERE CONTRACTOR'S INVESTIGATION CANNOT DETERMINE THE PROPER ADJUSTMENTS NEEDED TO MEET THE INTENT OF THE DESIGN, CONTRACTOR SHALL INFORM ARCHITECT.
- 2. EXISTING CIRCUITS AND HOMERUNG WERE BASED ON EXISTING DOCUMENTS.
- 3. REMOVED EQUIPMENT SHALL MAINTAIN CIRCUIT CONTINUITY FOR DEVICES / EQUIPMENT CONNECTED TO THE SAME CIRCUIT. EXTEND AND/OR REPOUTE THE EXISTING CIRCUITS AS NEEDED.
- 4. REVISE EXISTING PANEL SCHEDULES TO REFLECT THE NEWLY CONNECTED LOADS AND SPARE CIRCUITS.
- 5. DO NOT REUSE ANY REMOVED MATERIALS SUCH AS CONDUIT, WIRING, AND BOXES,
- 6. PRIOR TO COMMENCEMENT OF WORK THE CONTRACTOR SHALL VERIFY AND DOCUMENT WITH THE OWNER THE PROPER FUNCTION AND PHYSICAL APPEARANCE OF EXISTING ELECTRICAL EQUIPMENT (DEVICES, LIGHTING, RECEPTACLES, ETC.) IN THE ROOM AND THE AREA OF WORK UNDER THIS CONTRACTOR. IF AFTER CONSTRUCTION ANY EXISTING EQUIPMENT IS DAMAGED OR DOES NOT FUNCTION PROPERLY. THE CONTRACTOR SHALL REPAIR OR REPLACE THE EQUIPMENT IN-KIND FOR PROPER FUNCTION AND APPEARANCE.

ELECTRICAL COMPONENT ANCHORAGE NOTE:

ALL ELECTRICAL COMPONENTS SHALL BE ANCHORED & INSTALLED PER THE DETAILS ON THE DSA APPROVED CONSTRUCTION DOCUMENTS. WHERE NO DETAILS IS INDICATED, THE FOLLOWING COMPONENTS SHALL BE ANCHORED OR BRACED TO MEET THE FORCE AND DISPLACEMENT REQUIREMENTS PRESCRIBED IN THE 2013 CBC, SECTIONS 1616A.1.18 THROUGH 1616A.1.26 AND ASCE 1-10 CHAPTER 6 AND 13.

- ALL PERMANENT EQUIPMENT AND COMPONENTS.
- ATTACHMENTS.

THE ATTACHMENT OF THE FOLLOWING ELECTRICAL COMPONENTS SHALL BE POSITIVELY ATTACHED TO THE STRUCTURE, BUT NEED NOT BE DETAILED ON THE PLANS. THESE COMPONENTS SHALL HAVE FLEXIBLE CONNECTIONS PROVIDED BETWEEN THE COMPONENT AND ASSOCIATED CONDUIT.

- THE COMPONENT. HUNG FROM A WALL.

FOR THOSE ELEMENTS THAT DO NOT REQUIRED DETAILS ON THE APPROVED DRAWINGS, THE INSTALLATION SHALL BE SUBJECT TO THE APPROVAL OF THE STRUCTURAL ENGINEER OF RECORD AND THE DSA DISTRICT STRUCTURAL ENGINEER. THE PROJECT INSPECTOR WILL VERIFY THAT ALL COMPONENTS & EQUIPMENT HAVE BEEN ANCHORED IN ACCORDANCE WITH ABOVE REQUIREMENTS.

ELECTRICAL DISTRIBUTION SYSTEM BRACING NOTE:

ELECTRICAL DISTRIBUTION SYSTEMS SHALL BE BRACED TO COMPLY WITH THE FORCES AND DISPLACEMENTS PRESCRIBED IN ASCE 1-10 SECTION 13.3 AS DEFINED IN ASCE 1-10 SECTION 13.6.8, 13.6.7, 13.6.5.6, AND 2013 CBC, SECTIONS 1616A.1.23, 1616A.1.24, 1616A.1.25 AND 1616A.1.26.

THE BRACING AND ATTACHMENTS TO THE STRUCTURE SHALL BE DETAILED ON THE APPROVED DRAWINGS OR THEY SHALL COMPLY WITH ONE OF THE OSHPD PRE-APPROVALS (OPM #) AS MODIFIED TO SATISFY ANCHORAGE REQUIREMENTS OF ACI 318, APPENDIX D.

COPIES OF THE MANUAL SHALL BE AVAILABLE ON THE JOBSITE PRIOR TO THE START OF HANGING AND BRACING OF THE ELECTRICAL DISTRIBUTION SYSTEMS.

THE STRUCTURAL ENGINEER OF RECORD SHALL VERIFY THE ADEQUACY OF THE STRUCTURE TO SUPPORT THE HANGER AND BRACE LOADS.

TERMINAL CABINET SCHEDULE									
	SIZE			MOUNTING					
DESIGNATION	Σ	Ħ	D	SURFACE	FLUSH	NEMA-1	NEMA-3R		
FATC-H	14"	24"	6"						
STC-H	4"	24"	6"						

NOTES:

- 1. ALL TERMINAL CABINETS SHALL BE NEMA-1 WITH HINGED DOORS, CYLINDER TYPE LOCKS, \$ 3/4" PLYWOOD BACKBOARD, U.O.N.
- 2. PROVIDE TERMINAL BLOCKS, TYPE AS REQUIRED.
- A. SIEMENS #66MI-50 WITH 89B STAND-OFF. MAKE FULL USE OF BRIDGE CLIPS.
- B. BUCHANAN #0525 SERIES. PROVIDE CHANNEL CLAMPS, CHANNEL AND END SECTIONS.

2. TEMPORARY OR MOVABLE EQUIPMENT THAT IS PERMANENTLY ATTACHED (E.G. HARD WIRED) TO THE BUILDING UTILITY SERVICES SUCH AS ELECTRICITY, GAS OR WATER. 3. MOVABLE EQUIPMENT WHICH IS STATIONED IN ONE PLACE FOR MORE THAN & HOURS AND HEAVIER THAN 400 POUNDS ARE REQUIRED TO BE ANCHORED WITH TEMPORARY

A. COMPONENTS WEIGHING LESS THAN 400 POUNDS AND HAVE A CENTER OF MASS LOCATED 4 FEET OR LEGS ABOVE THE ADJACENT FLOOR OR ROOF LEVEL THAT DIRECTLY SUPPORT

B. COMPONENTS WEIGHING LESS THAN 20 POUNDS, OR IN THE CASE OF DISTRIBUTED SYSTEMS, LESS THAN 5 POUNDS PER FOOT, WHICH ARE SUSPENDED FROM A ROOF OR FLOOR OR

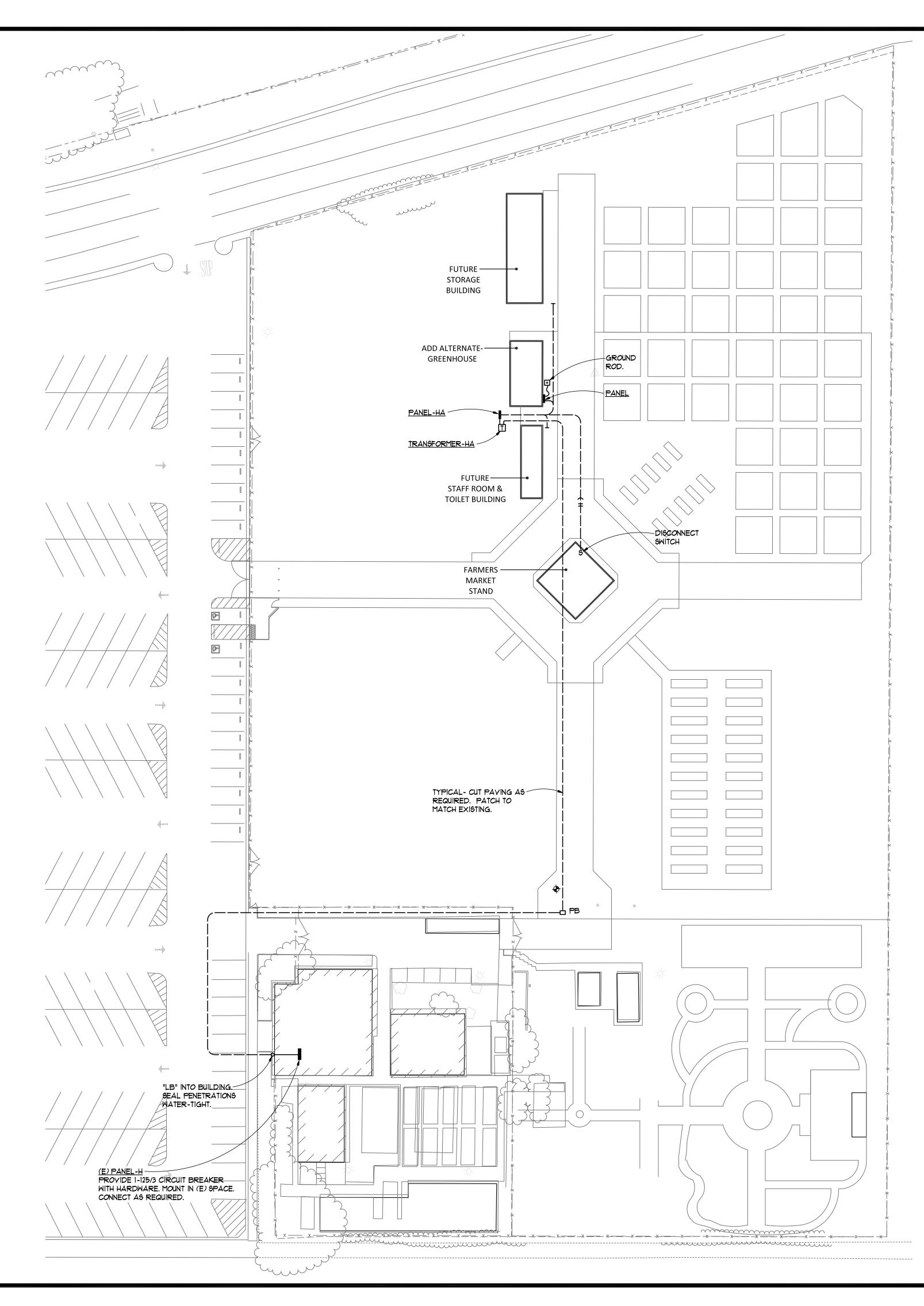
POWER AND SIGNAL SYSTEMS DURING CONSTRUCTION

- POWER AND SIGNAL SYSTEMS: SYSTEMS SHUT-DOWNS SHALL BE COORDINATED WITH THE OWNER. SYSTEMS DOWN TIME SHALL OCCUR ONLY ON THE WEEKENDS AND DURING "OFF" HOURS. THE WEEKEND SHALL BE DEFINED AS FROM 5:00 PM FRIDAY TO THE NEXT 6:00 AM MONDAY. "OFF" HOURS SHALL BE DEFINED AS FROM 5:00 PM EVENING TO 6:00 AM THE NEXT MORNING. NORMAL BUSINESS HOURS SHALL BE DEFINED AS 6:00 AM MONDAY TO 5:00 PM FRIDAY WITHIN THE SAME WEEK. DURING BUSINESS HOURS, POWER SHALL BE PROVIDED AND SIGNAL SYSTEMS SHALL BE OPERATIONAL TO THE CAMPUS.
- 2. SIGNAL SYSTEMS SHALL INCLUDE TELECOR INTERCOM, PAGING, CLOCK SYSTEM, ADEMCO INTRUSION, DATA, VOIP TELEPHONE, TELEVISION, AND HARRINGTO FIRE ALARM.
- 3. THROUGHOUT CONSTRUCTION, THE ELECTRICAL AND SIGNAL SYSTEMS SHALL REMAIN IN OPERATION.
- 4. SIGNAL SYSTEMS: PROVIDE DEVICES AS SHOWN ON THE DRAWINGS AND ALL NECESSARY EQUIPMENT INCLUDING HARDWARE, WIRING AND PROGRAMMING FOR A COMPLETE AND OPERATIONAL SYSTEM PER SCHOOL DISTRICT REQUIREMENTS. COORDINATE WITH SCHOOL DISTRICT FOR SYSTEM OPERATIONS PRIOR TO BID. TEST SYSTEM TO COMPLY WITH MANUFACTURER'S OPERATION REQUIREMENTS. DEVICES AND EQUIPMENT ADDITIONS SHALL NOT VOID THE EXISTING EQUIPMENT WARRANTY.
- 5. LOCAL FIRE AUTHORITY SHALL BE NOTIFIED 48 HOURS IN ADVANCE OF FIRE ALARM SHUT DOWN.

		ARCHITECT
	ELECTRICAL SYMBOLS LIST	
	CONDUIT CONCEALED BELOW FLOOR OR GRADE.	ARCHITECTURE + PLANNIN G
	CONDUIT CONCEALED IN CEILING OR WALL. HOMERUN TO RESPECTIVE PANEL OR TERMINAL.	333 1ST STREET, SUITE C SAN FRANCISCO, CA 94105 303 POTRERO STREET, SUITE 7B
	INDICATES 1#12 (GREEN) GROUND WIRE; OTHER SIZES AS INDICATED.	SANTA CRUZ, CA 95060
NOTE:	BRANCH CIRCUIT WITHOUT FURTHER DESIGNATION IS A 2#12 WIRE CIRCUIT. FOR MORE THAN 2#12 WIRES AS FOLLOWS: ————————————————————————————————————	TEL: 800.725.0571 OWNER
۲	10 6 PULL-BOX WITH GROUND ROD, SEE DETAIL.	
_ , _	PANELBOARD, SEE SCHEDULE.	
□ ₽	TERMINAL CABINET BACKBOARD. JUNCTION BOX.	SOLANO COMMUNITY COLLEGE
•	15 AMP DOUBLE DUPLEX RECEPTACLE MOUNT IN IDF.	COMMUNITY COLLEGE
⊖ FATC	15 AMP DUPLEX RECEPTACLE, +18".	SOLANO COMMUNITY COLLEGE DISTRICT 4000 Suisun Valley Rd, Fairfield, CA 94534
	FIRE ALARM TERMINAL CABINET. TRANSFORMER	CONSULTANT
Sup	WEATHERPROOF SINGLE POLE DISCONNECT SWITCH, TOGGLE TYPE WITH LOCKING COVER, +45".	HARRY A. YEE &
<1 (E) ====	NUMBER CONSTRUCTION NOTES SPECIFIC TO THE SHEET. EXISTING PANELBOARD.	ASSOCIATES, INC. ELECTRICAL ENGINEERS 4920 FREEPORT BOULEVARD
(E)	ABBREVIATION FOR EXISTING.	No. E14987 Fyn 6/30/17
GND	ABBREVIATION FOR GROUND.	
N.I.E.S.	ABBREVIATION FOR NOT IN ELECTRICAL SECTIONS OF THESE PLANS AND SPEC'S.	STATE OF CALIFORNIA HYA Job #1612C
STC	ABBREVIATION FOR SIGNAL TERMINAL CABINET.	PROFESSIONAL STAMP:
WP	ABBREVIATION FOR WEATHERPROOF.	
		[T
		PROJECT:
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		PLANT SCIENCE
		BUILDINGS
		4000 Suisun Valley Rd, [] Fairfield, CA 94534
		REVISIONS
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		- DSA SUBMITTAL 3/7/16
		PROJECT CODE: SCCD-04 START DATE: -
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		ELECTRICAL
		SYMBOL LIST
		DSA APPROVAL STAMP:

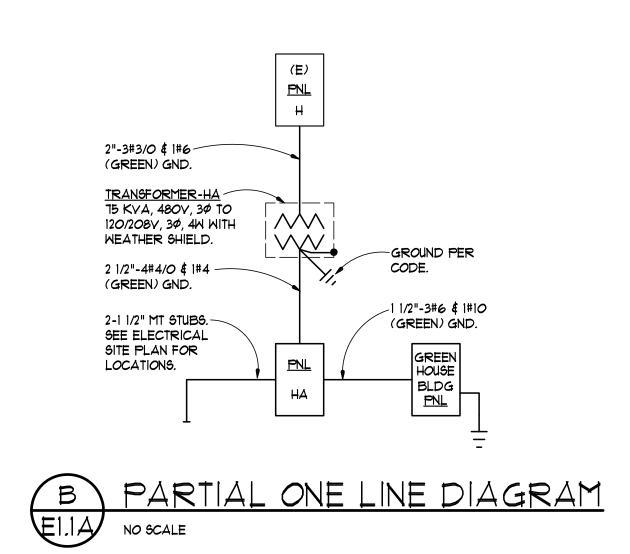
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GND | MINIMU TYPE: MOUNT MISC: 1 KVA





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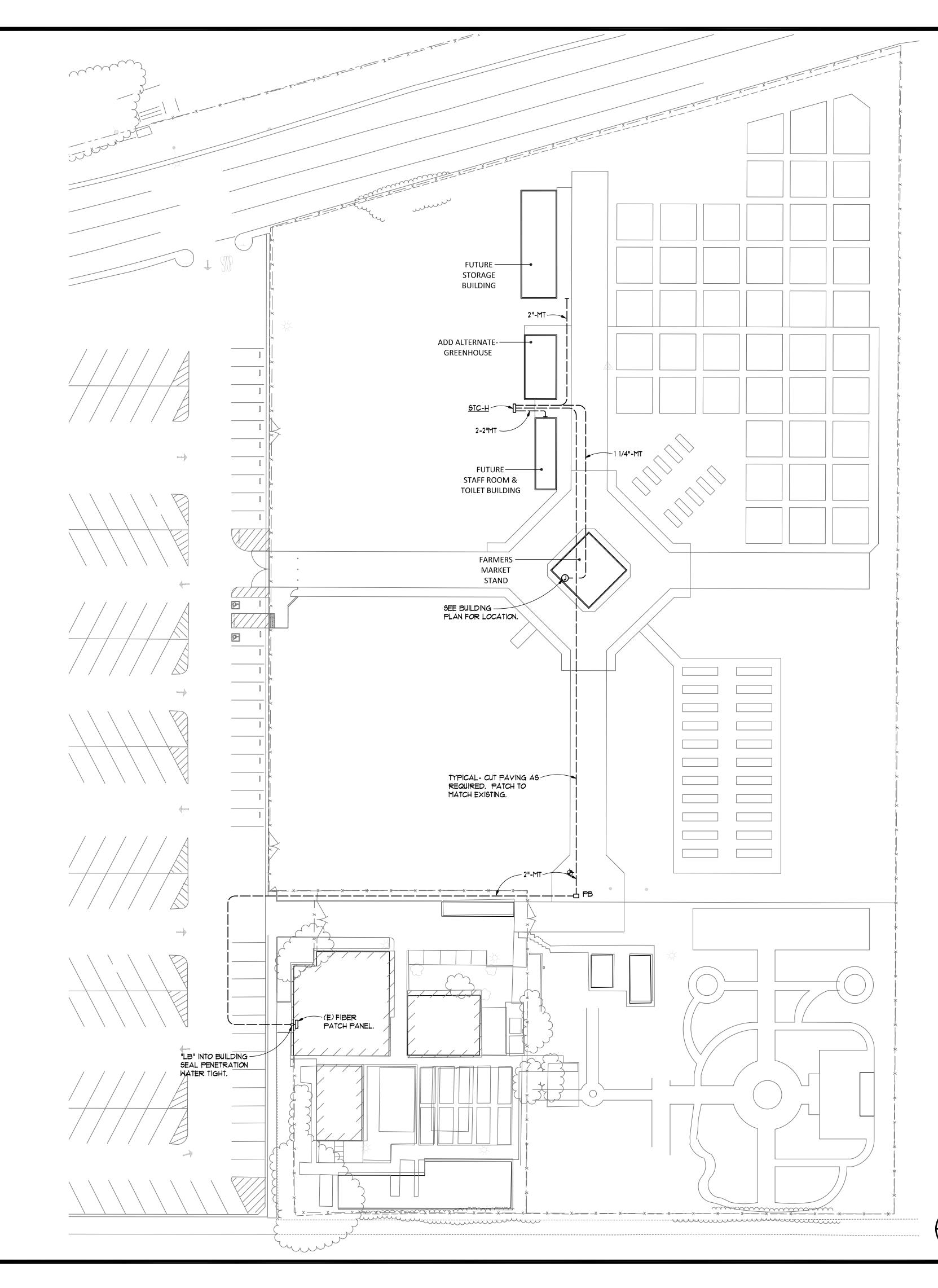
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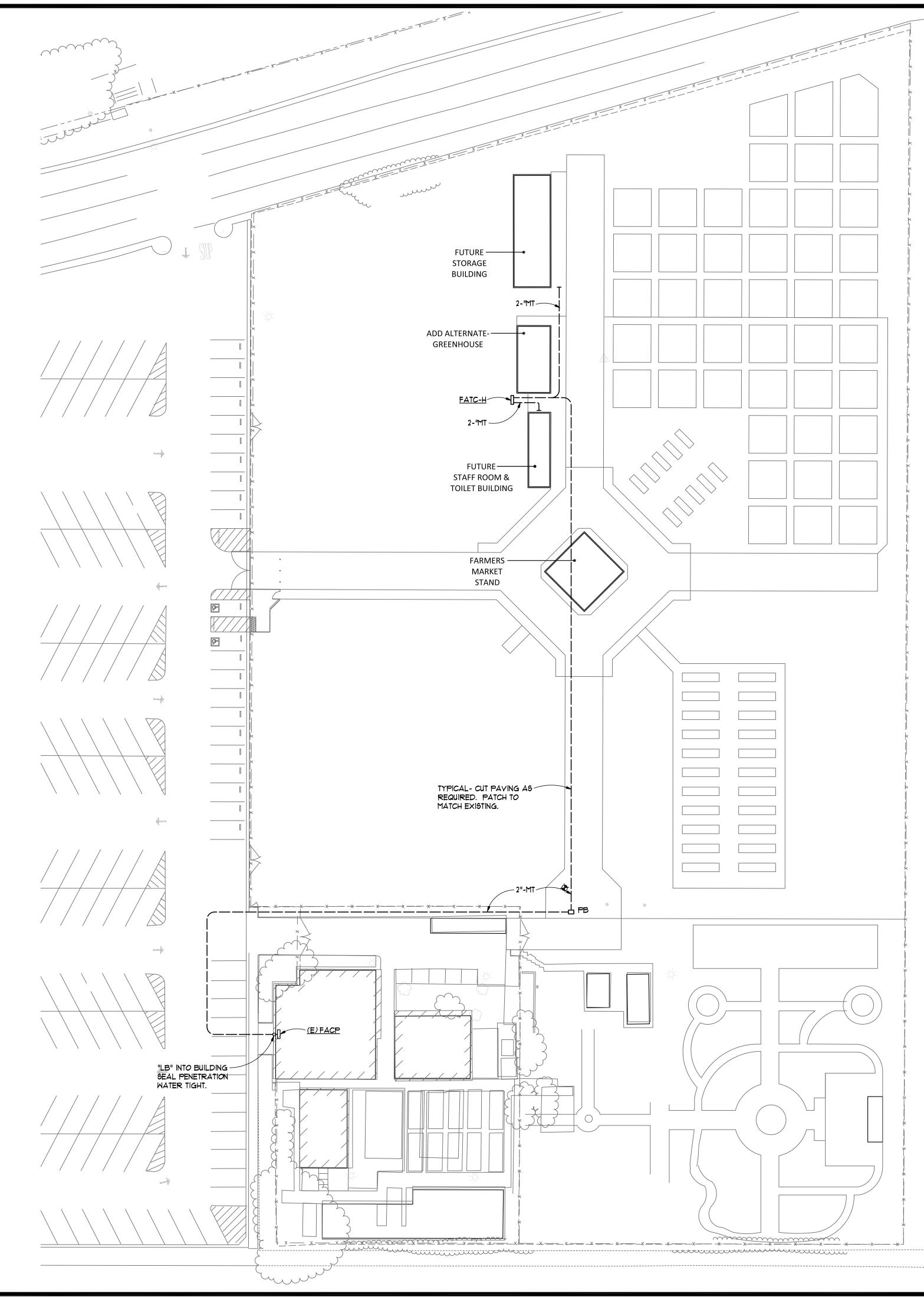
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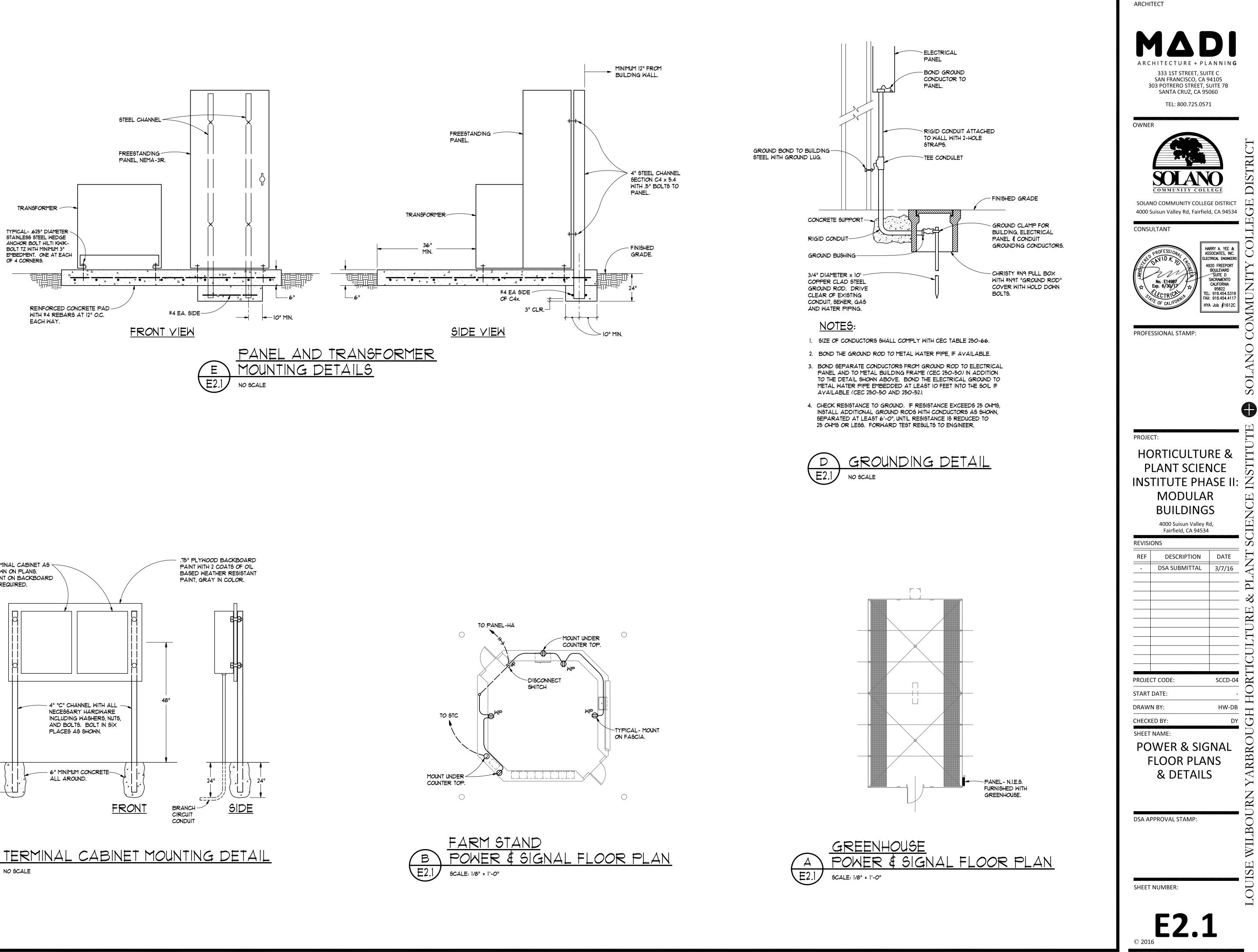


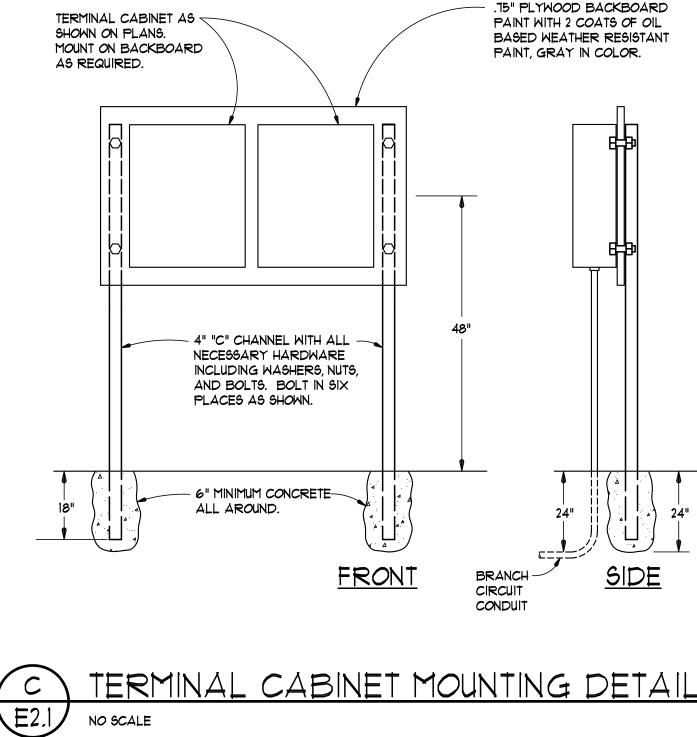


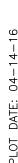


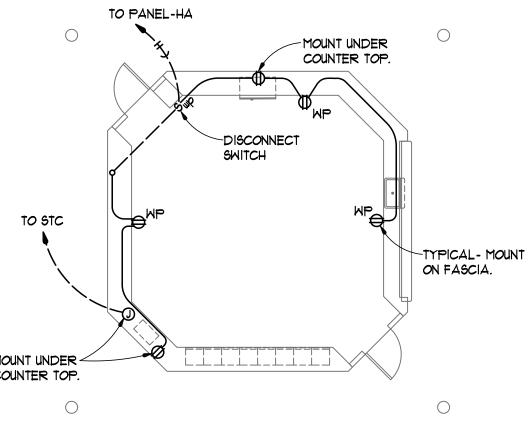
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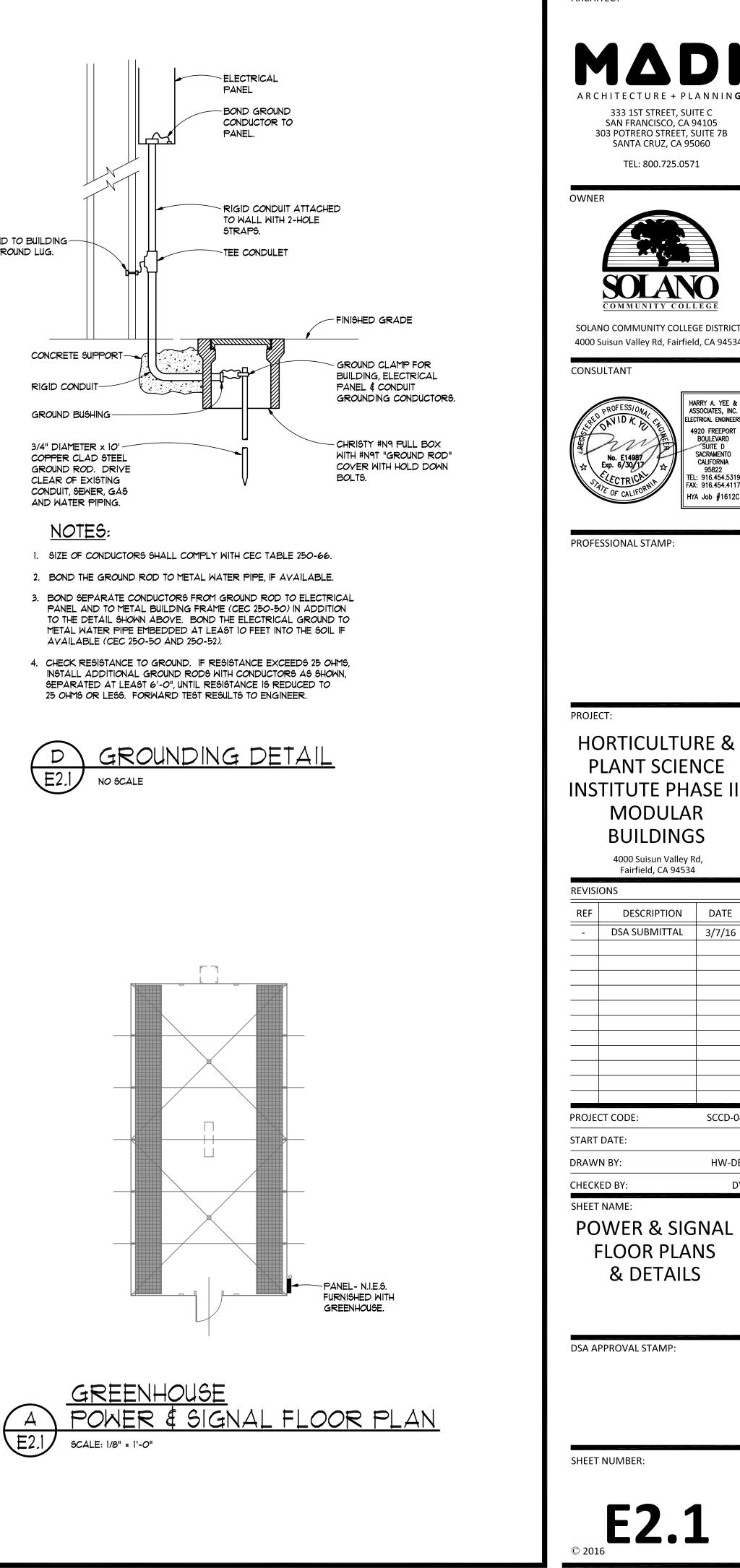


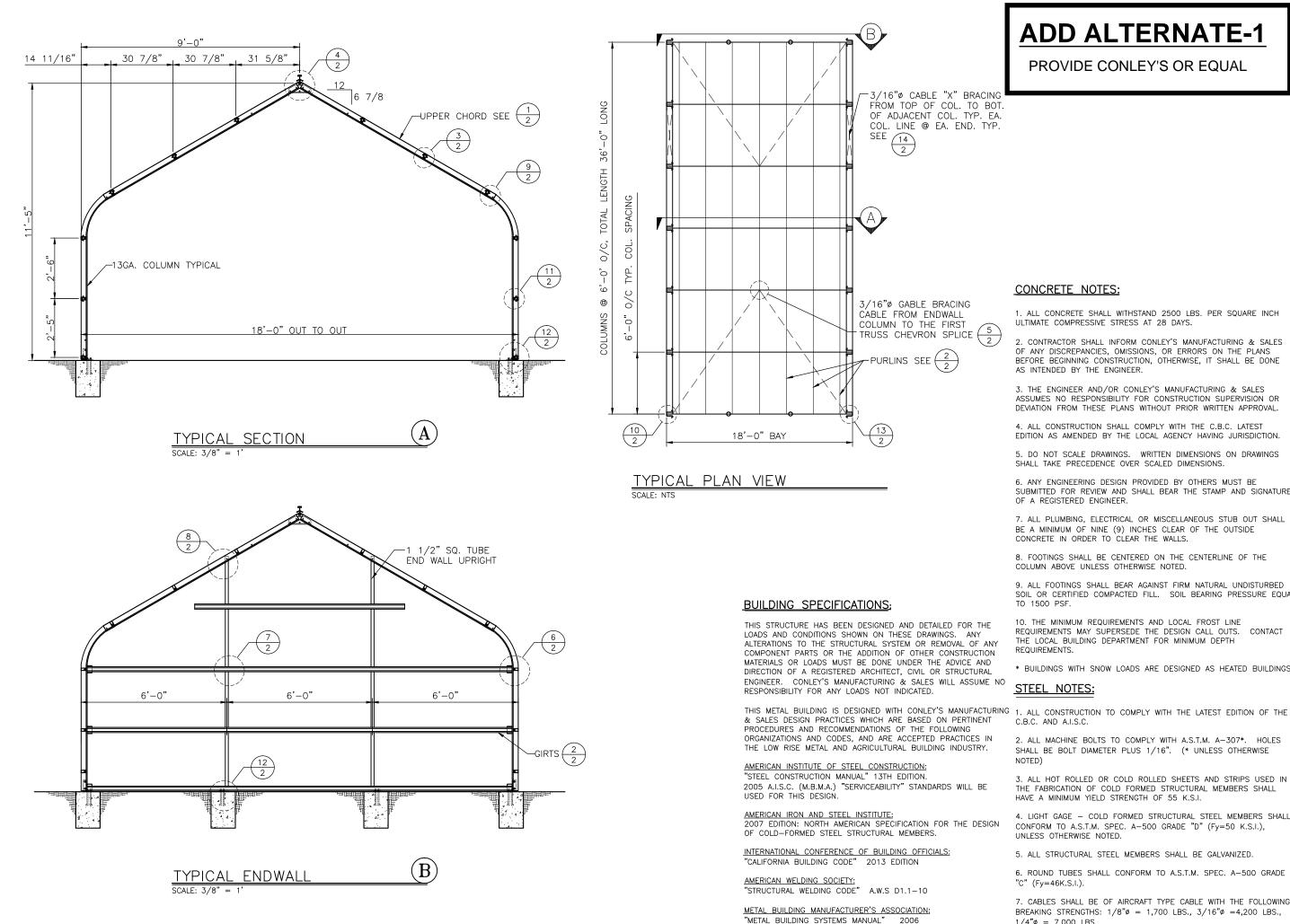












ADD ALTERNATE-1

PROVIDE CONLEY'S OR EQUAL

CONCRETE NOTES:

1. ALL CONCRETE SHALL WITHSTAND 2500 LBS. PER SQUARE INCH ULTIMATE COMPRESSIVE STRESS AT 28 DAYS.

CONTRACTOR SHALL INFORM CONLEY'S MANUFACTURING & SALES OF ANY DISCREPANCIES, OMISSIONS, OR ERRORS ON THE PLANS BEFORE BEGINNING CONSTRUCTION, OTHERWISE, IT SHALL BE DONE AS INTENDED BY THE ENGINEER.

3. THE ENGINEER AND/OR CONLEY'S MANUFACTURING & SALES ASSUMES NO RESPONSIBILITY FOR CONSTRUCTION SUPERVISION OR DEVIATION FROM THESE PLANS WITHOUT PRIOR WRITTEN APPROVAL.

4. ALL CONSTRUCTION SHALL COMPLY WITH THE C.B.C. LATEST EDITION AS AMENDED BY THE LOCAL AGENCY HAVING JURISDICTION.

5. DO NOT SCALE DRAWINGS. WRITTEN DIMENSIONS ON DRAWINGS SHALL TAKE PRECEDENCE OVER SCALED DIMENSIONS.

6. ANY ENGINEERING DESIGN PROVIDED BY OTHERS MUST BE SUBMITTED FOR REVIEW AND SHALL BEAR THE STAMP AND SIGNATURE OF A REGISTERED ENGINEER.

7. ALL PLUMBING, ELECTRICAL OR MISCELLANEOUS STUB OUT SHALL BE A MINIMUM OF NINE (9) INCHES CLEAR OF THE OUTSIDE CONCRETE IN ORDER TO CLEAR THE WALLS.

8. FOOTINGS SHALL BE CENTERED ON THE CENTERLINE OF THE COLUMN ABOVE UNLESS OTHERWISE NOTED.

9. ALL FOOTINGS SHALL BEAR AGAINST FIRM NATURAL UNDISTURBED SOIL OR CERTIFIED COMPACTED FILL. SOIL BEARING PRESSURE EQUAL TO 1500 PSF.

10. THE MINIMUM REQUIREMENTS AND LOCAL FROST LINE REQUIREMENTS MAY SUPERSEDE THE DESIGN CALL OUTS. CONTACT THE LOCAL BUILDING DEPARTMENT FOR MINIMUM DEPTH REQUIREMENTS.

* BUILDINGS WITH SNOW LOADS ARE DESIGNED AS HEATED BUILDINGS

STEEL NOTES:

C.B.C. AND A.I.S.C.

2. ALL MACHINE BOLTS TO COMPLY WITH A.S.T.M. A-307*. HOLES SHALL BE BOLT DIAMETER PLUS 1/16". (* UNLESS OTHERWISE

3. ALL HOT ROLLED OR COLD ROLLED SHEETS AND STRIPS USED IN THE FABRICATION OF COLD FORMED STRUCTURAL MEMBERS SHALL HAVE A MINIMUM YIELD STRENGTH OF 55 K.S.I.

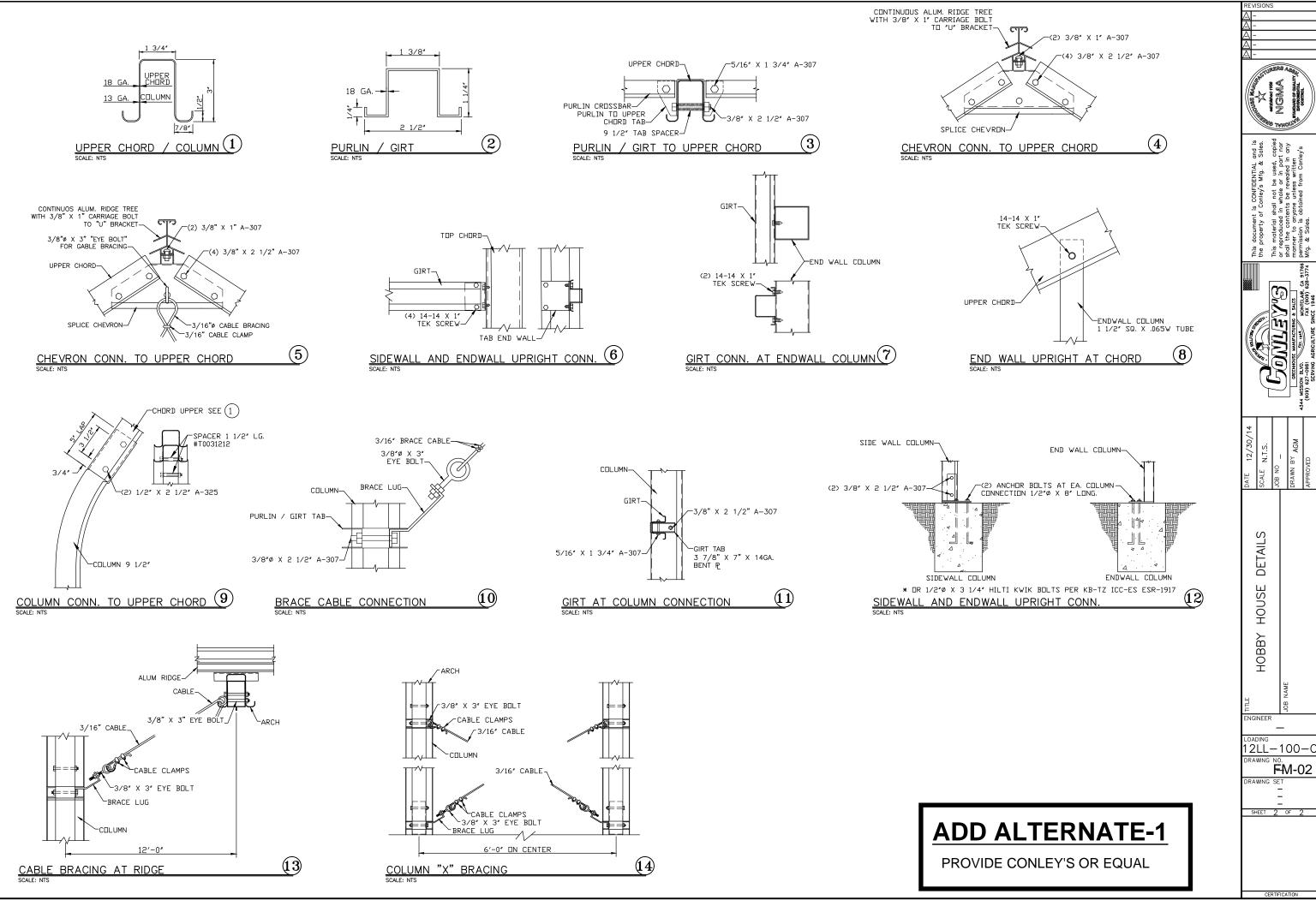
4. LIGHT GAGE - COLD FORMED STRUCTURAL STEEL MEMBERS SHALL CONFORM TO A.S.T.M. SPEC. A-500 GRADE "D" (Fy=50 K.S.I.), UNLESS OTHERWISE NOTED.

5. ALL STRUCTURAL STEEL MEMBERS SHALL BE GALVANIZED.

6. ROUND TUBES SHALL CONFORM TO A.S.T.M. SPEC. A-500 GRADE "C" (Fv=46K.S.I.).

7. CABLES SHALL BE OF AIRCRAFT TYPE CABLE WITH THE FOLLOWING BREAKING STRENGTHS: 1/8"¢ = 1,700 LBS., 3/16"¢ =4,200 LBS., $1/4"\phi = 7.000$ LBS.

		, JAN	A STANDARD OF QUALITY A	Control.
This document is CONFIDENTIAL and is	the property of Conley's Mfg. & Sales.	This material shall not be used, copied or reproduced in whole or in part nor	manner to anyone unless written	Mfg. & Sales.
and a strong the		$S_{\lambda} \neq h (0 C_{1})$		(90) 827-081 FX (90) 828-3774 Mfg. & Soles.
DATE 12/30/14	SCALE N.T.S.	- ON BOD	DRAWN BY AGM	APPROVED
	18' X 36' HOBBY HOUSE			
ENG LOAI DRA DRA			2	C
		RTIFIC		



EXAMPLE FORM DSA 103

NOTE: THE EXAMPLE FORM DSA-103 SHOWN ON THIS SHEET IS FOR ILLUSTRATION PURPOSES ON FUTURE PROJECT SPECIFIC FORM DSA-103'S. A FORM DSA-103 IS TO BE COMPLETED FOR EACH A INCORPORATED INTO AND THE EXAMPLE FORM DSA-103 IS TO BE CROSSED OUT ON THIS DRAWIN

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	Note: References are to the	2013 edition of the		
/.	REQUIRED TEST OR SPECIAL INSPECTION	TYPE	PERFORM	EP
12	SOILS			and an
	1. GENERAL:	Table 1705A.	.6	
X	 a. Verify that: site has been prepared properly prior to placement of controlled fill and/or excavations for foundations, foundation excavations are extended to proper depth and have reached proper material, and materials below footings are adequate to achieve the design bearing capacity. 	Periodic	GE*	* By geotechnical engineer GE for the site specific pro
*	2. COMPACTED FILLS:	Table 1705A.	.6 Lab*	* Under the supervision of
X	 a. Perform qualification testing of fill materials. b. Verify use of proper materials and inspect lift thicknesses, 	Test		* Under the supervision of * By geotechnical engineer
X	placement, and compaction during placement of fill.	Continuous	GE*	GE for the site specific pro
<u> </u>	c. Test compaction of fill. 4. CAST-IN-PLACE DEEP FOUNDATIONS (PI		Table 17	
X	a. Inspect drilling operations and maintain complete and accurate	Continuous	GE*	* By geotechnical engineer
X	records for each pier. b. Verify locations of piers.	Continuous	PI	GE for the site specific pro
X	 c. Confirm pier diameters, plumbness, bell diameters (if applicable), lengths, and embedment into bedrock (if applicable). Record concrete or grout volumes. 	Continuous	GE*	* By geotechnical engineer GE for the site specific pro
X	d. Confirm adequate end strata bearing capacity.	Test	Lab*	* Under the supervision of
Х	e. Concrete piers.		nd inspectio	ns per CONCRETE section b
	CONCRETE	Table 1705A.3		
54	7. CAST IN PLACE CONCRETE			513.507.007
X	A Verify use of required design mix.	Periodic	SI & PI*	* To be performed by batch
x	c. Perform slump, temperature, and (where required)	Test	Lab	ASTM C172, ASTM C31.
X	air content tests. d. Test concrete (compression).	Test	Lab	ACI 318 Section 5.6 and 7
	Inspection:		1	
X	e. Batch plant inspection	Continuous	SI	1705A.3.2; If approved by with 1705A.3.3, Item 1, and
X	 g. Inspect placement of formwork, reinforcing steel, embedded items and concrete. Inspect curing and form removal. 	Continuous	PI*	* May be performed by a s
-	MASONRY	TMS 402-11/AC	CI 530-11/A	SCE 5-11 Table 1.19.3
27 3	STEEL	Table 1705A.2.	.1	
-	17. STRUCTURAL STEEL AND COLD-FORME	D STEEL USE	D FOR	STRUCTURAL PUR
	Material Verification:			
X	 a. Verify that all materials are appropriately marked and that: Mill certificates indicate material properties that comply with requirements, 	Periodic	*	* By special inspector when project site without welding
X X	 Material sizes, types and grades comply with requirements. b. Test unidentified materials c. Examine seam welds of structural tubes and pipes 	Test Periodic	Lab Si*	2203A.1 (2203.1 ⁺). ASTM /
~ *	Inspection:			
X	 d. Verify member locations, bracing and all details constructed in the field. 	Continuous	PI	
X	 e. Verify stiffener locations, connection tab locations and all construction details fabricated in the shop. 	Periodic	SI	
-	18. HIGH STRENGTH BOLTS:			
	Material Verification of High-Strength Bolts, Nuts, and Was a. Verify identification markings and manufacturer's certificates of	hers:	1	1
X	compliance conform to ASTM standards specified in the DSA approved documents.	Periodic	SI	DSA IR 17-9
X	b. Test high-strength bolts, nuts and washers.	Test	Lab	2213A.1 (2212.6.1 ⁺). ASTM
चर	Inspection of High-Strength Bolt Installation:	-		
X	 c. Bearing-type ("snug tight") connections. 19. WELDING: 	Periodic	SI*	DSA IR 17-9 DSA IR 17-3, AWS D1.1 a
	Verification of Materials, Equipment, Welders, etc:			
X	a. Verify weld filler material identification markings per AWS	Periodic	SI	
	 designation listed on the DSA approved documents and the WPS. b. Verify weld filler material manufacturer's certificate of 	Devie die	CI	
X.	compliance.	Periodic	SI	
X	c. Verify WPS, welder qualifications and equipment. 19.1 SHOP WELDING:	Periodic	SI	DSA IR 17-3.
X	a. Inspect groove, multi-pass, and fillet welds > 5/16"	Continuous	SI	Per AISC 360 (and AISC 3
X	b. Inspect single-pass fillet welds ≤ 5/16"	Periodic	SI	Per AISC 360 (and AISC 3
	WOOD			
- }	OTHER			
1 2 3 4	Soils testing and Inspection: Geotechnical Verified Report - Form DSA-293 All Structural Testing: Laboratory Verified Report - Form DSA-291 Concrete Batch Plant Inspection: Special Inspection Verified Report - Form HS Bolt Installation Inspection: Special Inspection Verified Report - Form D	1 DSA-292		
KEY	to Columns			
-	Туре -		2 Perfe	ormed By -
Conti	nuous - Indicates that a continuous special inspection is required	-		ates that the special inspection representative
				cates that the test or inspection

	SI –	Indicates	that the	e special	inspecti
Shelter Optio	ns				

Periodic – Indicates that a periodic special inspection is required

Test – Indicates that a test is required

	Available Options	5		
Chaltan Stude				
Shelter Style				
	Length	Width		
20' Meramec	30', 42'			
30' Meramec	42', 54'			
16' Navajo				
20' Navajo				
24' Navajo				
30' Navajo				
36' Navajo				
40' Navajo				
1111-1	13' to 58' in 9'	10', 16'		
Illini	increments.	5.		
	9'-8" to 55'-8" in			
7' Shawnee	7'-8"			
	increments.			

OR	M DS	SA 10)3	nar penint in 1201 2000 and an ann			
	_				I THE COMPLETIC		
	LETED FO			TION TH	AT THIS PC IS BEI	NG	
	ı Building Co	ode (CBC)	unless oth	erwise note			
PERFOR	AED /	/					
PERFO							
M. 00					- 	NT (DECAMA	
				8-04-A 8-8-8-04 8-			
	* By geote	chnical end	ineer or his	or her qualif	fied representative. Use	PI in lieu of GE if	there is no
GE*	1	site specifi		1			
					,		
Lab*	* Under th	e supervisio	on of the ge	otechnical er	ngineer.		
GE*		chnical eng		or her qualif	fied representative. Us	e PI in lieu of GE if	there is no
Lab*	* Under th			otechnical er	ngineer.	NV7 977 W K	
able 17 GE*	* By geote	_		or her qualif	ied representative. Us	e PI in lieu of GE if	there is no
PI	GE for the	site specifi	c project.				
GE*	1	chnical eng		or her qualif	ied representative. Us	e PI in lieu of GE if	there is no
Lab*		-		otechnical er	ngineer.		
spectio	ons per CON	CRETE sec	tion below.	and the second	and the second		
51 & PI*	* To be pe	rformed by	batch-nlant	special insp	ector and project inspe	ctor.	
Lab		72, ASTM C					
Lab	ACI 318 S	ection 5.6	and 1905A	.1.2 (1913.3.	1 [⁺]). ASTM C3 <u>9</u> .		
<u> </u>	1705A.3.2	; If approve	ed by DSA.	batch plant i	nspection may be redu	ced to periodic if pl	ant complies
SI	with 1705/	A.3.3, Item	1, and requi	res first batc	h inspection, weighma	ster, and batch tick	
PI*				inspector wh	en specifically approve	ed by DSA.	
30-11/A	SCE 5-11 T	able 1.19.3			NU ADMINISTRATION NO AMERICAN		
FOR	STRUCT		PURPOS	SES			
*			when perfo elding or fab		e; by project inspector f	or steel shipped dir	ectly to
Lab		2203.1 ⁺). As					
SI*	* DSA IR 1			5			
PI			C94				
SI						<u> </u>	
			603340-004-0-01484				
SI	DSA IR 17	′-9					
Lab	2213A.1 (2	2212.6.1 ⁺)	ASTM F606	8, A370. DS/	A IR 17-8		
SI*	DSA IR 17		1.1.2.2.0.00				1
	USA IR 17	-3, AWS D	1.1 and AVV	S D1.8 (AVV	S D1.3 for cold formed		
SI							
SI		Creation and an and a second					
SI	DSA IR 17	/-3	Loomage.		9000		
SI			_		DSA IR 17-3.		
SI	Per AISC	360 (and Al	SC 341 as	applicable).	DSA IR 17-3.		
		<u> </u>	<u></u>				
						201 1000 (1 1000	
	formed By -						
thorized	t representati	ve	-	-	ed by a registered geot		
			•		ed by a testing laborato e section 4-335, 2013 (•	
					d by the project inspect		
	ates that the s	special insp	ection is to	be performe	d by a special inspecto	F	
5 Availa	able Option	s					
			Eave	Height			"∨" plugs
1	Length	Width	Min.	Max.	Recessed Anchor Bolts./Footings	Roof Downspouts	for bird control.
3	30', 42'		7'	12'	Y/N	Y/N	Y/N
4	12', 54'		<u>7'</u> 7'	12' 12'	Y/N Y/N	Y/N Y/N	Y/N Y/N
			7'	12'	Y/N	Y/N	Y/N
			<u>7'</u> 7'	12' 12'	Y/N Y/N	Y/N Y/N	Y/N Y/N
			7'	12'	Y/N	Y/N	Y/N
13' t	to 58' in 9'	101 4	7'	12'	Y/N	Y/N	Y/N
inc	rements.	10', 16'	7'-6"	12'	Y/N	Y/N	Y/N
ש-ע"	to 55'-8" in 7'-8"		7'-6"	12'	Y/N	Y/N	Y/N
	rements.						

2013 CBC PC STRUCTU	RAL DESIGN NOTES
SCRIPTION	DESIGN VALUES
DEAD AND LIVE LOADS	
ROOF LIVE LOAD (Lr) ROOF DEAD LOAD (D)	20 PSF 5 PSF
ALLOWABLE SOIL PRESSURE	
DL	1000 PSF
DL+Lr DL+SNOW	1000 PSF 1000 PSF
GROUND SNOW LOAD (Pg)	22 PSF
SLOPED ROOF SNOW LOAD (Ps)	20 PSF
SNOW EXPOSURE FACTOR (Ce) SNOW IMPORTANCE FACTOR (I)	1.1
THERMAL FACTOR (Ct)	1.2
FLOOD DESIGN	
FLOOD HAZARD AREA	NO
WIND DESIGN	
ULTIMATE DESIGN WIND SPEED (Vult) WIND EXPOSURE FACTOR	130 MPH C
TOPOGRAPHIC FACTOR (Kzt)	1.0
ASCE 7-10 WIND ANALYSIS METHOD	CHAPTER 27 DIRECTIONAL PROCEDURE
VELOCITY PRESSURE EXPOSURE COEFFICIENT (Kz)	0.85 VARIES, SEE CALCULATIONS
WIND DIRECTIONALITY FACTOR (Kd)	0.85
WIND VELOCITY PRESSURE (qh)	31.3 PSF
	1
ASCE 7-10 ANALYSIS PROCEDURE SEISMIC DESIGN CATEGORY	E SECTION 12.8 EQUIVALENT LATERAL FORCE PROCEDURE
SEISMIC IMPORTANCE FACTOR	1.0 D
MAPPED MCE, 5% DAMPED, SPECTRAL RESPONSE ACCELERATION AT SHORT PERIOD (Ss)	1.875
SHORT PERIOD SITE COEFFICIENT (Fa)	1.0
DESIGN MCE, 5% DAMPED, SPECTRAL RESPONSE ACCELERATION AT SHORT PERIOD (SDS)	1.0
MAPPED MCE, 5% DAMPED, SPECTRAL RESPONSE ACCELERATION AT 1 SECOND PERIOD (S1) LONG PERIOD SITE COEFFICIENT (Fv)	1.3
DESIGN, 5% DAMPED, SPECTRAL RESPONSE ACCELERATION AT 1 SECOND PERIOD (SD1)	1.3
HORIZONTAL OR VERTICAL IRREGULARITY TYPES	NONE
BUILDING	ΠΔΤΔ
CONSTRUCTION CLASSIFICATION	TYPE II-B
OCCUPANCY CLASSIFICATION RISK CATEGORY	A-2
NUMBER OF STORIES	1
SHEET	
G.1 AMERICANA SHELTERS I 10' AND 16' ILLINI SHELTER	DESIGN NOTES, EXAMPLE FORM DSA 103
□ IT.0 ILLINI SHELTER DESIGN □ IT.1 ILLINI SHELTER PLANS, S	NOTES, EXAMPLE FORM DSA 103 SECTIONS AND DETAILS
20' MERAMEC SHELTERS	
	DESIGN NOTES, EXAMPLE FORM DSA 103 PLANS, SECTIONS AND DETAILS
30' MERAMEC SHELTERS	DESIGN NOTES, EXAMPLE FORM DSA 103
MT30.1 30' MERAMEC SHELTER I	PLANS, SECTIONS AND DETAILS
16' NAVAJO SHELTERS □ NT16.0 16' NAVAJO SHELTER DE	SIGN NOTES, EXAMPLE FORM DSA 103
NT16.1 16' NAVAJO SHELTER PL/ 20' NAVAJO SHELTERS	ANS, SECTIONS AND DETAILS
	SIGN NOTES, EXAMPLE FORM DSA 103
 NT20.0 20' NAVAJO SHELTER DE NT20.1 NT20.2 NAVAJO SHELTER PL NT20.2 NAVAJO SHELTER SE 	
☐ NT20.1 20' NAVAJO SHELTER PL ☐ NT20.2 20' NAVAJO SHELTER SE 24' NAVAJO SHELTERS	CTIONS AND DETAILS
 NT20.1 20' NAVAJO SHELTER PL/ NT20.2 20' NAVAJO SHELTER SE 24' NAVAJO SHELTERS NT24.0 24' NAVAJO SHELTER DE NT24.1 24' NAVAJO SHELTER PL/ 	CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103 ANS AND ELEVATIONS
 NT20.1 20' NAVAJO SHELTER PL/ NT20.2 20' NAVAJO SHELTER SE 24' NAVAJO SHELTERS NT24.0 24' NAVAJO SHELTER DE 	CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103 ANS AND ELEVATIONS
 NT20.1 20' NAVAJO SHELTER PL NT20.2 20' NAVAJO SHELTER SE 24' NAVAJO SHELTERS NT24.0 24' NAVAJO SHELTER DE NT24.1 24' NAVAJO SHELTER PL NT24.2 24' NAVAJO SHELTER SE 30' NAVAJO SHELTERS NT30.0 30' NAVAJO SHELTER DE 	CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103 ANS AND ELEVATIONS CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103
 NT20.1 20' NAVAJO SHELTER PL/ NT20.2 20' NAVAJO SHELTER SE 24' NAVAJO SHELTERS NT24.0 24' NAVAJO SHELTER DE NT24.1 24' NAVAJO SHELTER PL/ NT24.2 24' NAVAJO SHELTER SE 30' NAVAJO SHELTERS NT30.0 30' NAVAJO SHELTER DE NT30.1 30' NAVAJO SHELTER PL/ NT30.2 30' NAVAJO SHELTER SE 	CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103 ANS AND ELEVATIONS CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103 ANS AND ELEVATIONS
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 NT20.1 20' NAVAJO SHELTER PL/ NT20.2 20' NAVAJO SHELTER SE 24' NAVAJO SHELTERS NT24.0 24' NAVAJO SHELTER DE NT24.1 24' NAVAJO SHELTER PL/ NT24.2 24' NAVAJO SHELTER SE 30' NAVAJO SHELTERS NT30.0 30' NAVAJO SHELTER DE NT30.1 30' NAVAJO SHELTER PL/ NT30.2 30' NAVAJO SHELTER SE 36' NAVAJO SHELTERS NT36.0 36' NAVAJO SHELTER DE NT36.1 36' NAVAJO SHELTER PL/ 	CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103 ANS AND ELEVATIONS CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103 ANS AND ELEVATIONS CTIONS AND DETAILS
 NT20.1 20' NAVAJO SHELTER PL NT20.2 20' NAVAJO SHELTER SE 24' NAVAJO SHELTERS NT24.0 24' NAVAJO SHELTER DE NT24.1 24' NAVAJO SHELTER PL NT24.2 24' NAVAJO SHELTER SE 30' NAVAJO SHELTERS NT30.0 30' NAVAJO SHELTER DE NT30.1 30' NAVAJO SHELTER PL NT30.2 30' NAVAJO SHELTER SE 36' NAVAJO SHELTERS NT36.0 36' NAVAJO SHELTER DE NT36.1 36' NAVAJO SHELTER PL NT36.2 36' NAVAJO SHELTER SE 40' NAVAJO SHELTERS 	CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103 ANS AND ELEVATIONS CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103 ANS AND ELEVATIONS CTIONS AND DETAILS SIGN NOTES, EXAMPLE FORM DSA 103 ANS AND ELEVATIONS CTIONS AND DETAILS
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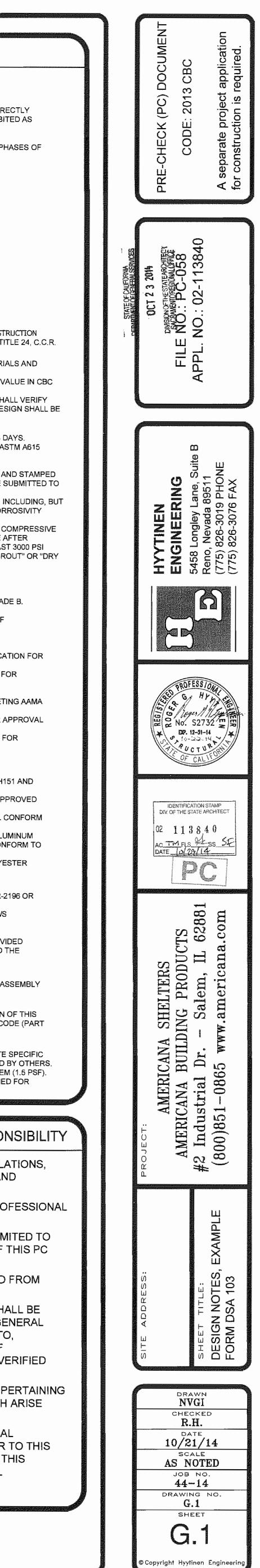
LI ST7.0 SHAWNEE SHELTER DESIGN NOTES, EXAMPLE FORM DSA 103 SHAWNEE SHELTER PLANS, SECTIONS AND DETAILS □ ST7.1

I.	SHELTER DESIGN A. THE STRUCTURAL DESIGN OF THE COMPONENTS AND CONNECTIONS C SUFFICIENT FOR EAVE HEIGHTS RANGING FROM 7' UP TO 12' TALL.	F THIS SHELTER ARE
	 B. REQUIRED EAVE HEIGHT FOR EACH SITE SHALL BE DETERMINED BY OW C. THIS SHELTER HAS BEEN DESIGNED AS AN OPEN STRUCTURE. THE ADD 	DITION OF ANY ENCLOSURE DIRECTL
11.		
	A. THE DESIGN OF THIS STRUCTURE IS IN CONFORMANCE WITH THE FOLL CONSTRUCTION SHALL BE PERFORMED IN ACCORDANCE WITH THE FOL	
	 2013 CALIFORNIA ADMINISTRATIVE CODE (CAC)	, TITLE 24, CCR)
	 2013 CALIFORNIA ELECTRICAL CODE	TITLE 24, CCR) IDMENTS)
	 2013 CALIFORNIA MECHANICAL CODE (CMC)	NDMENTS)
	(2012 UNIFORM PLUMBING CODE WITH 2013 CALIFORNIA AMENDI 6. 2013 CALIFORNIA ENERGY CODE	MENTS) TLE 24, CCR)
	 2013 CALIFORNIA FIRE CODE (CFC)	MENTS)
	9. 2013 CALIFORNIA REFERENCED STANDARDS CODE	
111.	11. NFPA 72 - 2013 CONSTRUCTION CHANGES A. CHANGES TO THE APPROVED PLANS AND SPECIFICATIONS SHALL BE M.	
IV.	CHANGE DOCUMENT APPROVED BY THE DIVISION OF THE STATE ARCHITE	
	 A. THE FOUNDATION SHALL REST ON SOUND SOIL THAT IS FREE OF ORGA CAPABLE OF SUPPORTING 1000 PSF VERTICAL BEARING PRESSURE. B. FOR LATERAL LOADING, THE FOUNDATION HAS BEEN DESIGNED TO THE 	
	TABLE 1806A.2. THIS IS 100 PSF/FT LATERAL BEARING. C. FOUNDATION DESIGN SHOWN IS BASED ON SOIL CONDITIONS GIVEN IN NO	TES A AND B, ABOVE, OWNER SHALL V
V.	ACTUAL SOIL CONDITIONS AT EACH JOB SITE AND ANY REQUIRED ADJU DESIGNED BY OTHERS. CONCRETE	STMENTS TO THE FOOTING DESIGN
•	 A. COMPRESSION STRENGTH OF ALL REINFORCED CONCRETE SHALL NOT B. REINFORCING BARS SHALL BE DEFORMED BARS CONFORMING TO THE 	REQUIREMENTS OF MINIMUM ASTM
	GRADE 40 FOR #4 AND SMALLER BARS AND GRADE 60 FOR BARS LARGE C. MINIMUM CONCRETE CLEAR COVER FOR REINFORCING BARS SHALL BE D. A CONCRETE MIX DESIGN IN ACCORDANCE WITH CBC SECTION CHAPTE	3".
	BY A CIVIL ENGINEER LICENSED IN THE STATE OF CALIFORNIA, THE CON THE INSPECTOR OF RECORD PRIOR TO CONSTRUCTION. E. THE MIX DESIGN SHALL MEET THE CRITERIA HEREIN AND SHALL BE PRO	
	NOT LIMITED TO, FREEZING AND THAWING EXPOSURE, CHEMICAL AND S WHERE SUCH PROBLEMS EXIST.	SALT EXPOSURE, AND SOIL CORROS
	F. NON-SHRINK GROUT OR DRY PACK SHALL BE A PREMIXED, NONMETALL STRENGTH OF 7000 PSI AT 28 DAYS AND HAVING THE FOLLOWING CHAR PLACEMENT OR EXPANSION AFTER SET (ASTM C1090), ONE DAY COMPR	ACTERISTICS: NO SHRINKAGE AFTE
	(ASTM C109) AND INITIAL SET TIME OF NOT LESS THAN 45 MINUTES (AST PACK GROUT" BY EUCLID, OR AN APPROVED EQUAL.	
VI.	A. STEEL PLATE SHALL CONFORM TO THE REQUIREMENTS OF ASTM A36.	
	 B. HOLLOW STRUCTURAL SECTIONS (HSS) SHALL CONFORM TO THE REQU C. ALL STRUCTURAL STEEL SHALL BE IDENTIFIED BY MILL CERTIFICATE. D. HIGH STRENGTH BOLTS (HSB) SHALL BE GALVANIZED AND SHALL CONFORMED 	
	ASTM A325-N. HIGH STRENGTH BOLTS SHALL BE TIGHTENED TO A SNUG ADDITIONAL HALF TURN. E. ALL HIGH STRENGTH BOLTS SHALL HAVE CERTIFICATION.	TIGHT CONDITION PLUS AN
	F. WELDING SHALL CONFORM TO THE REQUIREMENTS OF THE AMERICAN THE MATERIAL BEING WELDED. ALL WELDING SHALL BE PERFORMED BY	AWS CERTIFIED WELDERS.
	 G. WELD ELECTRODES SHALL BE E70XX AND SHALL CONFORM TO THE REC DEMAND CRITICAL WELDS. H. ALL WELDING SHALL BE APPROVED BY AN AWS CERTIFIED INSPECTOR. 	QUIREMENTS OF AWS D1.8-6.3 FOR
	 STEEL FRAMING SHALL BE COATED WITH ANTI-GRAFFITI POLYESTER TG 2604-02 SPECIFICATIONS. SHOP DRAWINGS OF ALL STRUCTURAL STEEL SHALL BE SUBMITTED TO 	
	PRIOR TO FABRICATION. K. ALL BOLT HOLE DIAMETERS SHALL BE EQUAL TO THE BOLT DIAMETER P	
VII	ANCHOR BOLTS SHALL BE EQUAL TO THE BOLT DIAMETER PLUS 1/8". L. ANCHOR BOLTS SHALL CONFORM TO ASTM F1554, GRADE 36 AND SHAL	L BE HOT DIP GALVANIZED.
γII.	 ALUMINUM A. INTERLOCKING SEAM ALUMINUM ROOF DECK SHALL BE ROLL FORMED F SHALL CONFORM TO THE DECK PROFILE SHOWN ON THE DRAWINGS. 	
	 B. ALUMINUM ROOF DECK SHALL BE COATED WITH HEAT REFLECTIVE BAS EQUAL. C. EXTRUDED ALUMINUM RIDGE CAP SHALL BE FABRICATED FROM ALUMIN 	
	TO THE REQUIREMENTS SHOWN ON THE DRAWINGS. D. EXTRUDED ALUMINUM FASCIA SHALL BE FABRICATED FROM ALUMINUM GUTTER SHAL BE FABRICATED FROM ALUMINUM ALLOY 6105-T5. ALUMI	
	THE REQUIREMENTS SHOWN ON THE DRAWINGS. E. EXTRUDED ALUMINUM RIDGE CAP, GUTTER, AND FASCIA SHALL BE COA	
VIII	TGIC POWDER COAT FINISH MEETING AAMA 2604-02 SPECIFICATIONS. I. SCREWS	
	 A. SCREWS SHALL BE HILTI KWIK-PRO SELF DRILLING SCREWS WITH BOND APPROVED EQUAL. B. SCREWS ATTACHING TO STEEL SHALL BE 12-24 HEX WASHER HEAD (HW 	
	ATTACHING TO ALUMINUM SHALL BE 8-18 HEX WASHER HEAD (HWH) #2 I C. ALL SCREWS SHALL BE STAINLESS STEEL OR COATED WITH ZINC. D. THE MANUFACTURER SHALL PROVIDE A SCREW CERTIFICATION LETTER	POINT SCREWS.
	MATCH THE SIZE AND TYPE SPECIFIED HEREIN. THE CERTIFICATION LET INSPECTOR OF RECORD PRIOR TO INSTALLATION.	
IX.	A. ALL STRUCTURAL STEEL AND ALUMINUM COMPONENTS SHALL BE SHOP	
Х.	OF CONNECTIONS CAN BE PERFORMED USING ONLY BOLTING AND SCR SPECIAL INSPECTION A. THE OWNER SHALL EMPLOY A SPECIAL INSPECTOR TO PERFORM INSPE	
	PC IN ACCORDANCE WITH THE REQUIREMENTS OF CHAPTER 17A OF THI 2, TITLE 24, C.C.R.) AND THE DIVISION OF THE STATE ARCHITECT.	
XI.	FIRE LIFE SAFETY A. AN AUTOMATIC FIRE PROTECTION SYSTEM MAY BE REQUIRED FOR THIS REQUIREMENTS. WHERE REQUIRED, THE AUTOMATIC FIRE PROTECTION	
	 B. THE DESIGN OF THIS SHELTER IS CAPABLE OF SUPPORTING THE WEIGH C. THE METAL ROOFING COMPLIES WITH FIRE CLASSIFICATION B. THIS SHI PLACEMENT WITHIN ANY FIRE HAZARD SEVERITY ZONE. 	T OF A FIRE SPRINKLER SYSTEM (1.
NOT	TICE OF DISCLAIMER FOR STRUCTURAL ENG	INEERING RESPONS
1.	PER TITLE 24, PART 1, SECTION 4-316(e) OF THE CALIFO	RNIA CODE OF REGULATIO
	THIS NOTICE SHALL BE GIVEN TO DSA PRIOR TO THE AP SPECIFICATIONS.	
2.	FOR THE SITE SPECIFIC PROJECT, ROGER HYYTINEN IS IN GENERAL RESPONSIBLE CHARGE, UNLESS NOTED O	
3.	FOR THE SITE SPECIFIC PROJECT, ROGER HYYTINEN'S	RESPONSIBILITY IS LIMITE
	THE PREPARATION OF PLANS AND SPECIFICATIONS FO ONLY.	R THE SHELTER(S) OF TH
4.	STRUCTURAL OBSERVATION OF CONSTRUCTION IS SPE ROGER HYYTINEN'S RESPONSIBILITY FOR THE SITE SPE	
5.	ALL CONSTRUCTION ACTIVITIES RELATED TO STRUCTU	RAL ENGINEERING SHALL
	DELEGATED TO A QUALIFIED ENGINEER BY THE DESIGN RESPONSIBLE CHARGE. THESE ACTIVITIES INCLUDE, BU	JT ARE NOT LIMITED TO,
	APPROVAL OF INSPECTOR QUALIFICATIONS, STRUCTUR CONSTRUCTION, REVIEW OF INSPECTION REPORTS, AN	
	REPORT FOR COMPLETED WORK.	

GENERAL NOTES

6. ROGER HYYTINEN WILL BE RESPONSIBLE FOR RESPONDING TO QUESTIONS PERTAINING TO THE PLANS AND SPECIFICATIONS FOR THE SHELTER(S) OF THIS PC WHICH ARISE DURING PLAN CHECK AND CONSTRUCTION.

7. IN THE EVENT THAT ROGER HYYTINEN IS REQUIRED TO PROVIDE STRUCTURAL OBSERVATION OF CONSTRUCTION, HE SHALL BE NOTIFIED IN WRITING PRIOR TO THIS REQUIREMENT BEING MADE. ALSO, HIS ANTICIPATED ADDITIONAL FEES FOR THIS ADDITIONAL WORK SHALL BE PAID IN ADVANCE, PRIOR TO ANY STRUCTURAL OBSERVATION OR CONSTRUCTION SERVICES BEING PERFORMED.



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	EXAMPLE	FOR	M DSA 103
			ION PURPOSES ONLY TO ASSIST IN THE COMPLETION OF ETED FOR EACH APPLICATION THAT THIS PC IS BEING
INCORPORATED INTO AND THE EXAMPLE FORM D			
	e to the 2013 edition of the	and the second second second	Building Code (CBC) unless otherwise noted.
ALCUIRED TEST OR SPECIAL INSPECTION	TYPE	PERFORM	
SOILS		1 24 B	
1. GENERAL:	Table 1705A.	6	
 a. Verify that: site has been prepared properly prior to placement of controlle fill and/or excavations for foundations, foundation excavations are extended to proper depth and have reached proper material, and materials below footings are adequate to achieve the design bearing capacity. 		GE*	* By geotechnical engineer or his or her qualified representative. Use PI in lieu of GE if there is no GE for the site specific project.
- 2. COMPACTED FILLS:	Table 1705A.	T	* Linder the supervision of the gestachnical engineer
 a. Perform qualification testing of fill materials. b. Verify use of proper materials and inspect lift thicknesses, 	Test	Lab* GE*	 * Under the supervision of the geotechnical engineer. * By geotechnical engineer or his or her qualified representative. Use PI in lieu of GE if there is no
placement, and compaction during placement of fill.	Continuous	Lab*	GE for the site specific project. * Under the supervision of the geotechnical engineer.
4. CAST-IN-PLACE DEEP FOUNDATION	S (PIERS):	Table 17	05A.7
a. Inspect drilling operations and maintain complete and accurate records for each pier.	Commuous	GE*	* By geotechnical engineer or his or her qualified representative. Use PI in lieu of GE if there is no GE for the site specific project.
 b. Verify locations of piers. c. Confirm pier diameters, plumbness, bell diameters (if 	Continuous	PI	* By geotechnical engineer or his or her qualified representative. Use PI in lieu of GE if there is no
applicable), lengths, and embedment into bedrock (if applicable) Record concrete or grout volumes.	e). Continuous	GE*	GE for the site specific project.
 d. Confirm adequate end strata bearing capacity. e. Concrete piers. 	Test Provide tests ar	Lab*	* Under the supervision of the geotechnical engineer.
- CONCRETE	Table 1705A.3		
7. CAST IN PLACE CONCRETE	AT EDISE DOTTOLE PROGRAMMENTALE OFFICE AND		
Material Verification and Testing: K a. Verify use of required design mix.	Periodic	SI & PI*	* To be performed by batch-plant special inspector and project inspector.
c. Perform slump, temperature, and (where required) air content tests.	Test	Lab	ASTM C172, ASTM C31.
d. Test concrete (compression).	Test	Lab	ACI 318 Section 5.6 and 1905A.1.2 (1913.3.1 ⁺). ASTM C39.
e. Batch plant inspection	Continuous	SI	1705A.3.2 ; If approved by DSA, batch plant inspection may be reduced to periodic if plant complies with 1705A.3.3 , Item 1, and requires first batch inspection, weighmaster, and batch tickets.
g. Inspect placement of formwork, reinforcing steel, embedded items and concrete. Inspect curing and form removal.	Continuous	PI*	* May be performed by a special inspector when specifically approved by DSA.
MASONRY	TMS 402-11/AC	CI 530-11/AS	SCE 5-11 Table 1.19.3
- STEEL	Table 1705A.2.		
- 17. STRUCTURAL STEEL AND COLD-FC Material Verification:	DRMED STEEL USE	ED FOR	STRUCTURAL PURPOSES
 a. Verify that all materials are appropriately marked and that: • Mill certificates indicate material properties that comply with requirements, 	Periodic	*	* By special inspector when performed off-site; by project inspector for steel shipped directly to project site without welding or fabrication.
Material sizes, types and grades comply with requirements. b. Test unidentified materials	Test	Lab	2203A.1 (2203.1 ⁺). ASTM A370.
c. Examine seam welds of structural tubes and pipes Inspection:	Periodic	SI*	* DSA IR 17-3.
 d. Verify member locations, bracing and all details constructed in the field. 	Continuous	PI	
e. Verify stiffener locations, connection tab locations and all construction details fabricated in the shop.	Periodic	SI	
- 18. HIGH STRENGTH BOLTS: Material Verification of High-Strength Bolts, Nuts, ar	d Washers		
a. Verify identification markings and manufacturer's certificates of	f	éi	DSA ID 17.0
compliance conform to ASTM standards specified in the DSA approved documents.	Periodic	SI	
b. Test high-strength bolts, nuts and washers. Inspection of High-Strength Bolt Installation:	Test	Lab	2213A.1 (2212.6.1 ⁺). ASTM F606, A370. DSA IR 17-8
c. Bearing-type ("snug tight") connections.	Periodic	SI*	DSA IR 17-9 DSA IR 17-3, AWS D1.1 and AWS D1.8 (AWS D1.3 for cold formed steel).
19. WELDING: Verification of Materials, Equipment, Welders, etc:		È	
a. Verify weld filler material identification markings per AWS designation listed on the DSA approved documents and the W	/PS. Periodic	SI	
 b. Verify weld filler material manufacturer's certificate of compliance. 	Periodic	SI	
c. Verify WPS, welder qualifications and equipment.	Periodic	SI	DSA IR 17-3.
Image: number of the sector	Continuous	SI	Per AISC 360 (and AISC 341 as applicable). DSA IR 17-3.
 X b. Inspect single-pass fillet welds ≤ 5/16" L MOOD 	Periodic	SI	Per AISC 360 (and AISC 341 as applicable). DSA IR 17-3.
+ WOOD + OTHER			
 Soils testing and Inspection: Geotechnical Verified Report - Form D All Structural Testing: Laboratory Verified Report - Form DSA-291 Concrete Batch Plant Inspection: Special Inspection Verified Report HS Bolt Installation Inspection: Special Inspection Verified Report - 	t - Form DSA-292		
EY to Columns			armad By
Type -			ormed By - ates that the special inspection is to be performed by a registered geotechnical engineer or his or her
ontinuous – Indicates that a continuous special inspection is required		authorized	representative cates that the test or inspection is to be performed by a testing laboratory accepted in the DSA
eriodic – Indicates that a periodic special inspection is required est – Indicates that a test is required		laboratory	Evaluation and Acceptance (LEA) Program. See section 4-335, 2013 CCR Title 24, Part 1.
		una Indiaa	tes that the special inspection is to be performed by the project inspector

2013 CBC PC STRUCTURA	L DESIG
DESCRIPTION	DESIGN V
DEAD AND LIVE LOADS	9940
ROOF LIVE LOAD (Lr)	20 PSF
ROOF DEAD LOAD (D)	5 PSF
ALLOWABLE SOIL PRESSURE	
DL	1000 PSF
DL+Lr	1000 PSF
DL+SNOW	1000 PSF
ROOF SNOW LOAD	
GROUND SNOW LOAD (Pg)	22 PSF
SLOPED ROOF SNOW LOAD (Ps)	20 PSF
SNOW EXPOSURE FACTOR (Ce)	1.1
SNOW IMPORTANCE FACTOR (I)	1.0
THERMAL FACTOR (Ct)	1.2
FLOOD DESIGN	1
FLOOD HAZARD AREA	NO
WIND DESIGN	
ULTIMATE DESIGN WIND SPEED (Vult)	130 MPH
WIND EXPOSURE FACTOR	С
TOPOGRAPHIC FACTOR (Kzt)	1.0
ASCE 7-10 WIND ANALYSIS METHOD	CHAPTER 27 I
VELOCITY PRESSURE EXPOSURE COEFFICIENT (Kz)	0.85
	VARIES, SEE
	0.85 31,3 PSF
WIND VELOCITY PRESSURE (qh)	31,3 - 3-
SEISMIC DESIGN	
LATERAL FORCE RESISTING SYSTEM	STEEL ORDIN
ASCE 7-10 ANALYSIS PROCEDURE	SECTION 12.8
SEISMIC DESIGN CATEGORY	E
SEISMIC IMPORTANCE FACTOR	1.0
DESIGN BASE SHEAR (V)	1305 #
SEISMIC RESPONSE COEFFICIENT (Cs)	0.29
RESPONSE MODIFICATION FACTOR (R)	3.5
SYSTEM OVERSTRENGTH FACTOR (Ω0)	3.0
DEFLECTION AMPLIFICATION FACTOR (Cd)	3.0
SITE CLASS	D
MAPPED MCE, 5% DAMPED, SPECTRAL RESPONSE ACCELERATION AT SHORT PERIOD (Ss)	1.875
SHORT PERIOD SITE COEFFICIENT (Fa)	1.0
DESIGN MCE, 5% DAMPED, SPECTRAL RESPONSE ACCELERATION AT SHORT PERIOD (SDS)	1.0
MAPPED MCE, 5% DAMPED, SPECTRAL RESPONSE ACCELERATION AT 1 SECOND PERIOD (S1)	1.3
LONG PERIOD SITE COEFFICIENT (Fv)	1.5
DESIGN, 5% DAMPED, SPECTRAL RESPONSE ACCELERATION AT 1 SECOND PERIOD (SD1)	1.3
HORIZONTAL OR VERTICAL IRREGULARITY TYPES	NONE

	BUILDING DATA		
CONSTRUCTION CLASSIFICATION		TYPE II-B	
OCCUPANCY CLASSIFICATION		A-2	
RISK CATEGORY		1	
NUMBER OF STORIES		1	
 MINIMUM SEISMIC SEPARATION		3"	
BUILDING AREA		900 SF	

NOTICE OF DISCLAIMER FOR STRUCTURAL ENGI

- 1. PER TITLE 24, PART 1, SECTION 4-316(e) OF THE CALIFORNIA CODE OF REGULATIONS, THIS NOTICE SHALL BE GIVEN TO DSA PRIOR TO THE APPROVAL OF PLANS AND SPECIFICATIONS.
- 2. FOR THE SITE SPECIFIC PROJECT, ROGER HYYTINEN IS NOT THE DESIGN PROFESSIONAL IN GENERAL RESPONSIBLE CHARGE, UNLESS OTHERWISE NOTED.
- FOR THE SITE SPECIFIC PROJECT, ROGER HYYTINEN'S RESPONSIBILITY IS 3. LIMITED TO THE PREPARATION OF PLANS AND SPECIFICATIONS FOR THE SHELTER(S) OF THIS PC ONLY.
- 4. STRUCTURAL OBSERVATION OF CONSTRUCTION IS SPECIFICALLY EXCLUDED FROM ROGER HYYTINEN'S RESPONSIBILITY FOR THE SITE SPECIFIC PROJECT.
- ALL CONSTRUCTION ACTIVITIES RELATED TO STRUCTURAL ENGINEERING SHALL BE DELEGATED TO A QUALIFIED ENGINEER BY THE DESIGN PROFESSIONAL IN GENERAL RESPONSIBLE CHARGE. THESE ACTIVITIES INCLUDE, BUT ARE NOT LIMITED TO, APPROVAL OF INSPECTOR QUALIFICATIONS, STRUCTURAL OBSERVATION OF CONSTRUCTION, REVIEW OF INSPECTION REPORTS, AND SIGNING OFF THE VERIFIED REPORT FOR COMPLETED WORK.
- ROGER HYYTINEN WILL BE RESPONSIBLE FOR RESPONDING TO QUESTIONS 6 PERTAINING TO THE PLANS AND SPECIFICATIONS FOR THE SHELTER(S) OF THIS PC WHICH ARISE DURING PLAN CHECK AND CONSTRUCTION.
- 7. IN THE EVENT THAT ROGER HYYTINEN IS REQUIRED TO PROVIDE STRUCTURAL OBSERVATION OF CONSTRUCTION, HE SHALL BE NOTIFIED IN WRITING PRIOR TO THIS REQUIREMENT BEING MADE. ALSO, HIS ANTICIPATED ADDITIONAL FEES FOR THIS ADDITIONAL WORK SHALL BE PAID IN ADVANCE, PRIOR TO ANY STRUCTURAL OBSERVATION OR CONSTRUCTION SERVICES BEING PERFORMED.

GN NOTES	
N VALUES	
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27 DIRECTIONAL PROCEDURE	
EE CALCULATIONS	
DINARY MOMENT RESISTING FRAMES	
DINARY MOMENT RESISTING FRAMES	EDURE
	EDURE
	EDURE

	GENERAL NOTES
l. II.	<ul> <li>SHELTER DESIGN</li> <li>A. THE STRUCTURAL DESIGN OF THE COMPONENTS AND CONNECTIONS OF THIS SHELTER ARE SUFFICIENT FOR EAVE HEIGHTS RANGING FROM 7' UP TO 12' TALL.</li> <li>B. REQUIRED EAVE HEIGHT FOR EACH SITE SHALL BE DETERMINED BY OWNER.</li> <li>C. THIS SHELTER HAS BEEN DESIGNED AS AN OPEN STRUCTURE. THE ADDITION OF ANY ENCLOSURE DIRECTLY ATTACHED TO THE SHELTER, SUCH AS WALLS, INSECT MESH, OR SHADE SCREENS, SHALL BE PROHIBITED AS INCREASED WIND FORCES MAY RESULT.</li> <li>DESIGN AND CONSTRUCTION STANDARDS</li> </ul>
	A. THE DESIGN OF THIS STRUCTURE IS IN CONFORMANCE WITH THE FOLLOWING STANDARDS AND ALL PHASES OF CONSTRUCTION SHALL BE PERFORMED IN ACCORDANCE WITH THE FOLLOWING STANDARDS.
	<ol> <li>2013 CALIFORNIA ADMINISTRATIVE CODE (CAC)</li></ol>
111.	CONSTRUCTION CHANGES A. CHANGES TO THE APPROVED PLANS AND SPECIFICATIONS SHALL BE MADE BY AN ADDENDA OR CONSTRUCTION
IV.	CHANGE DOCUMENT APPROVED BY THE DIVISION OF THE STATE ARCHITECT AS REQUIRED BY PART 1, TITLE 24, C.C FOUNDATION
	<ul> <li>A. THE FOUNDATION SHALL REST ON SOUND SOIL THAT IS FREE OF ORGANIC AND DELETERIOUS MATERIALS AND CAPABLE OF SUPPORTING 1000 PSF VERTICAL BEARING PRESSURE.</li> <li>B. FOR LATERAL LOADING, THE FOUNDATION HAS BEEN DESIGNED TO THE MINIMUM LATERAL BEARING VALUE IN CETABLE 1806A.2. THIS IS 100 PSF/FT LATERAL BEARING.</li> <li>C. FOUNDATION DESIGN SHOWN IS BASED ON SOIL CONDITIONS GIVEN IN NOTES A AND B, ABOVE. OWNER SHALL VERIFY ACTUAL SOIL CONDITIONS AT EACH JOB SITE AND ANY REQUIRED ADJUSTMENTS TO THE FOOTING DESIGN SHAL DESIGNED BY OTHERS.</li> </ul>
V.	<ul> <li>CONCRETE</li> <li>A. COMPRESSION STRENGTH OF ALL REINFORCED CONCRETE SHALL NOT BE LESS THAN 4000 PSI AT 28 DAYS.</li> <li>B. REINFORCING BARS SHALL BE DEFORMED BARS CONFORMING TO THE REQUIREMENTS OF MINIMUM ASTM A615 GRADE 40 FOR #4 AND SMALLER BARS AND GRADE 60 FOR BARS LARGER THAN #4.</li> <li>C. MINIMUM CONCRETE CLEAR COVER FOR REINFORCING BARS SHALL BE 3".</li> <li>D. A CONCRETE MIX DESIGN IN ACCORDANCE WITH CBC SECTION CHAPTER 19A SHALL BE PERFORMED AND STAMP BY A CIVIL ENGINEER LICENSED IN THE STATE OF CALIFORNIA. THE CONCRETE MIX DESIGN SHALL BE SUBMITTED THE INSPECTOR OF RECORD PRIOR TO CONSTRUCTION.</li> <li>E. THE MIX DESIGN SHALL MEET THE CRITERIA HEREIN AND SHALL BE PROPER FOR LOCAL CONDITIONS INCLUDING NOT LIMITED TO, FREEZING AND THAWING EXPOSURE, CHEMICAL AND SALT EXPOSURE, AND SOIL CORROSIVITY WHERE SUCH PROBLEMS EXIST.</li> <li>F. NON-SHRINK GROUT OR DRY PACK SHALL BE A PREMIXED, NONMETALLIC FORMULA WITH A MINIMUM COMPRESS STRENGTH OF 7000 PSI AT 28 DAYS AND HAVING THE FOLLOWING CHARACTERISTICS: NO SHRINKAGE AFTER PLACEMENT OR EXPANSION AFTER SET (ASTM C1090), ONE DAY COMPRESSIVE STRENGTH OF AT LEAST 3000 PSI (ASTM C109) AND INITIAL SET TIME OF NOT LESS THAN 45 MINUTES (ASTM C191). PROVIDE "HI-FLOW GROUT" OR "I PACK GROUT" BY EUCLID, OR AN APPROVED EQUAL.</li> </ul>
∨I.	<ul> <li>STRUCTURAL STEEL</li> <li>A. STEEL PLATE SHALL CONFORM TO THE REQUIREMENTS OF ASTM A36.</li> <li>B. HOLLOW STRUCTURAL SECTIONS (HSS) SHALL CONFORM TO THE REQUIREMENTS OF ASTM A500, GRADE B.</li> <li>C. ALL STRUCTURAL STEEL SHALL BE IDENTIFIED BY MILL CERTIFICATE.</li> <li>D. HIGH STRENGTH BOLTS (HSB) SHALL BE GALVANIZED AND SHALL CONFORM TO THE REQUIRMENTS OF ASTM A325-N. HIGH STRENGTH BOLTS SHALL BE TIGHTENED TO A SNUG TIGHT CONDITION PLUS AN ADDITIONAL HALF TURN.</li> <li>E. ALL HIGH STRENGTH BOLTS SHALL HAVE CERTIFICATION.</li> <li>F. WELDING SHALL CONFORM TO THE REQUIREMENTS OF THE AMERICAN WELDING SOCIETY'S SPECIFICATION FOR THE MATERIAL BEING WELDED. ALL WELDING SHALL BE PERFORMED BY AWS CERTIFIED WELDERS.</li> <li>G. WELD ELECTRODES SHALL BE E70XX AND SHALL CONFORM TO THE REQUIREMENTS OF AWS D1.8-6.3 FOR DEMAND CRITICAL WELDS.</li> <li>H. ALL WELDING SHALL BE APPROVED BY AN AWS CERTIFIED INSPECTOR.</li> <li>I. STEEL FRAMING SHALL BE COATED WITH ANTI-GRAFFITI POLYESTER TGIC POWDER COAT FINISH MEETING AAMA 2604-02 SPECIFICATIONS.</li> <li>J. SHOP DRAWINGS OF ALL STRUCTURAL STEEL SHALL BE SUBMITTED TO HYYTINEN ENGINEERING FOR APPROVAL</li> </ul>
	PRIOR TO FABRICATION. K. ALL BOLT HOLE DIAMETERS SHALL BE EQUAL TO THE BOLT DIAMETER PLUS 1/16" U.N.O. BOLT HOLES FOR
	ANCHOR BOLTS SHALL BE EQUAL TO THE BOLT DIAMETER PLUS 1/8". L. ANCHOR BOLTS SHALL CONFORM TO ASTM F1554, GRADE 36 AND SHALL BE HOT DIP GALVANIZED.
₩1.	<ul> <li>ALUMINUM</li> <li>A. INTERLOCKING SEAM ALUMINUM ROOF DECK SHALL BE ROLL FORMED FROM ALUMINUM ALLOY 3004-H151 AND SHALL CONFORM TO THE DECK PROFILE SHOWN ON THE DRAWINGS.</li> <li>B. ALUMINUM ROOF DECK SHALL BE COATED WITH HEAT REFLECTIVE BASF ULTRA-COOL COATING OR APPROVED EQUAL.</li> <li>C. EXTRUDED ALUMINUM RIDGE CAP SHALL BE FABRICATED FROM ALUMINUM ALLOY 6105-T5 AND SHALL CONFORM TO THE REQUIREMENTS SHOWN ON THE DRAWINGS.</li> <li>D. EXTRUDED ALUMINUM FASCIA SHALL BE FABRICATED FROM ALUMINUM ALLOY 6063-T5. EXTRUDED ALUMINUM GUTTER SHAL BE FABRICATED FROM ALUMINUM ALLOY 6105-T5. ALUMINUM COMPONENTS SHALL CONFORM TO THE REQUIREMENTS SHOWN ON THE DRAWINGS.</li> <li>E. EXTRUDED ALUMINUM RIDGE CAP, GUTTER, AND FASCIA SHALL BE COATED WITH ANTI-GRAFFITI POLYESTER TGIC POWDER COAT FINISH MEETING AAMA 2604-02 SPECIFICATIONS.</li> </ul>
VIII.	SCREWS
	<ul> <li>A. SCREWS SHALL BE HILTI KWIK-PRO SELF DRILLING SCREWS WITH BOND SEAL WASHERS PER ICC ESR-2196 OR APPROVED EQUAL.</li> <li>B. SCREWS ATTACHING TO STEEL SHALL BE 12-24 HEX WASHER HEAD (HWH) #5 POINT SCREWS. SCREWS ATTACHING TO ALUMINUM SHALL BE 8-18 HEX WASHER HEAD (HWH) #2 POINT SCREWS.</li> <li>C. ALL SCREWS SHALL BE STAINLESS STEEL OR COATED WITH ZINC.</li> <li>D. THE MANUFACTURER SHALL PROVIDE A SCREW CERTIFICATION LETTER STATING THAT SCREWS PROVIDED MATCH THE SIZE AND TYPE SPECIFIED HEREIN. THE CERTIFICATION LETTER SHALL BE SUBMITTED TO THE INSPECTOR OF RECORD PRIOR TO INSTALLATION.</li> </ul>
IX.	SHOP FABRICATION AND FIELD ASSEMBLY A. ALL STRUCTURAL STEEL AND ALUMINUM COMPONENTS SHALL BE SHOP FABRICATED SO THAT FIELD ASSEMBLY
X.	OF CONNECTIONS CAN BE PERFORMED USING ONLY BOLTING AND SCREW PLACEMENT. SPECIAL INSPECTION A. THE OWNER SHALL EMPLOY A SPECIAL INSPECTOR TO PERFORM INSPECTION OF THE CONSTRUCTION OF THIS PC IN ACCORDANCE WITH THE REQUIREMENTS OF CHAPTER 17A OF THE 2013 CALIFORNIA BUILDING CODE (PART 2, TITLE 24, C.C.R.) AND THE DIVISION OF THE STATE ARCHITECT.
XI.	<ul> <li>FIRE LIFE SAFETY</li> <li>A. AN AUTOMATIC FIRE PROTECTION SYSTEM MAY BE REQUIRED FOR THIS BUILDING DEPENDING ON SITE SPECIFIC REQUIREMENTS. WHERE REQUIRED, THE AUTOMATIC FIRE PROTECTION SYSTEM SHALL BE DESIGNED BY OTHER</li> <li>B. THE DESIGN OF THIS SHELTER IS CAPABLE OF SUPPORTING THE WEIGHT OF A FIRE SPRINKLER SYSTEM (1.5 PSF)</li> <li>C. THE METAL ROOFING COMPLIES WITH FIRE CLASSIFICATION B. THIS SHELTER HAS NOT BEEN DESIGNED FOR PLACEMENT WITHIN ANY FIRE HAZARD SEVERITY ZONE.</li> </ul>
 	SITE SPECIFIC OPTIONS
	TO BE COMPLETED PRIOR TO PLAN CHECK SUBMITTAL.          QUANTITY OF SHELTERS OF THIS PC AT THIS SITE
	CONCRETE SLAB OR ASPHALT PAVING (BY OTHERS) OVER FOOTINGS?  YES NO ROOF DOWNSPOUTS? ALUMINUM "V" PLUGS IN ROOF VOIDS FOR BIRD CONTROL? YES NO

### SHEET INDEX

NT30.0 30' NAVAJO SHELTER DESIGN NOTES, EXAMPLE FORM DSA 103 NT30.1 30' NAVAJO SHELTER PLANS AND ELEVATIONS

NT30.2 30' NAVAJO SHELTER SECTIONS AND DETAILS

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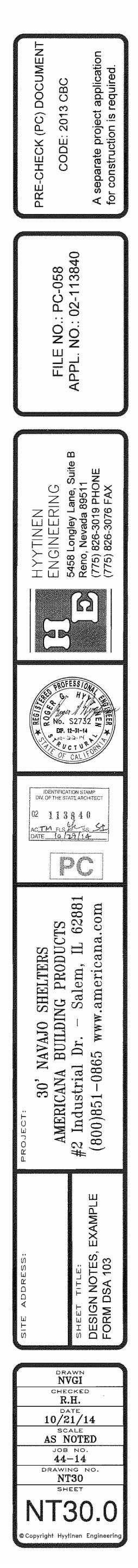
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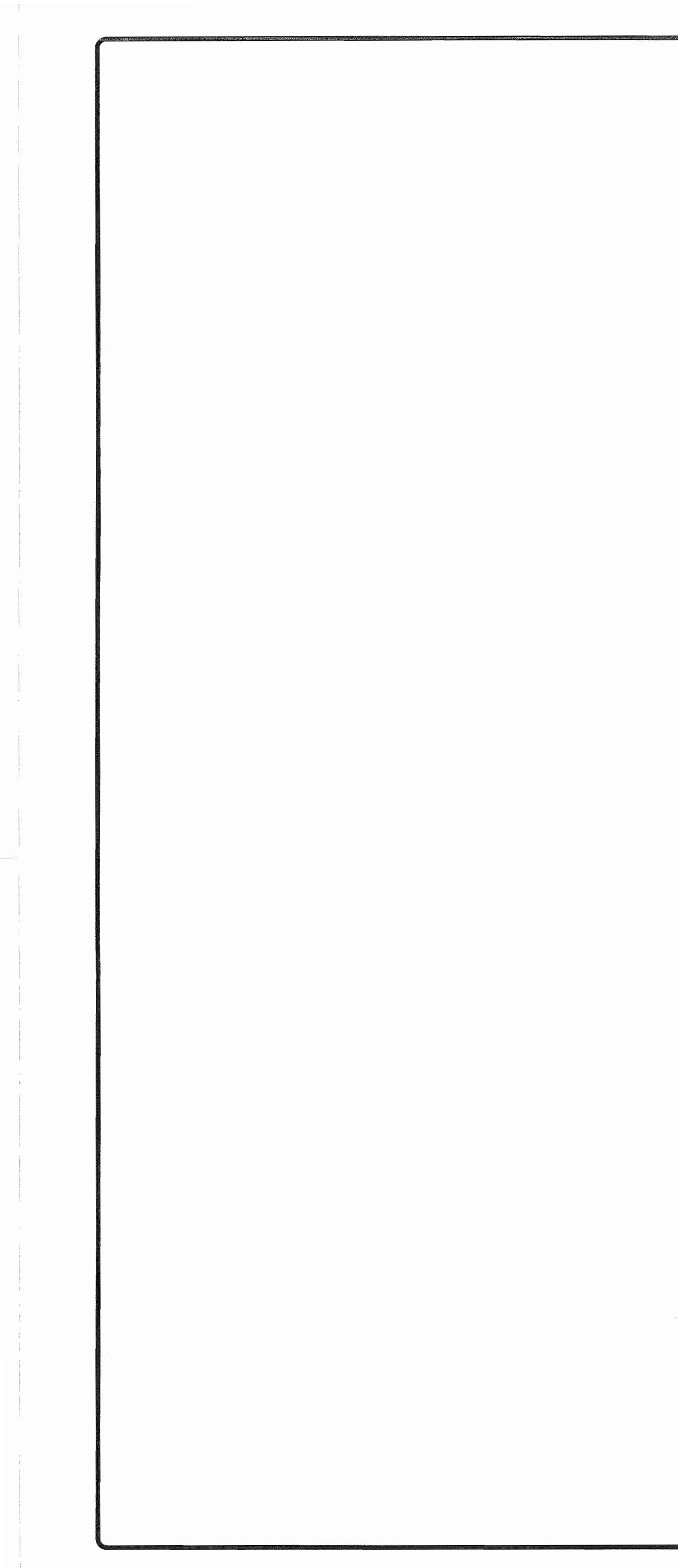
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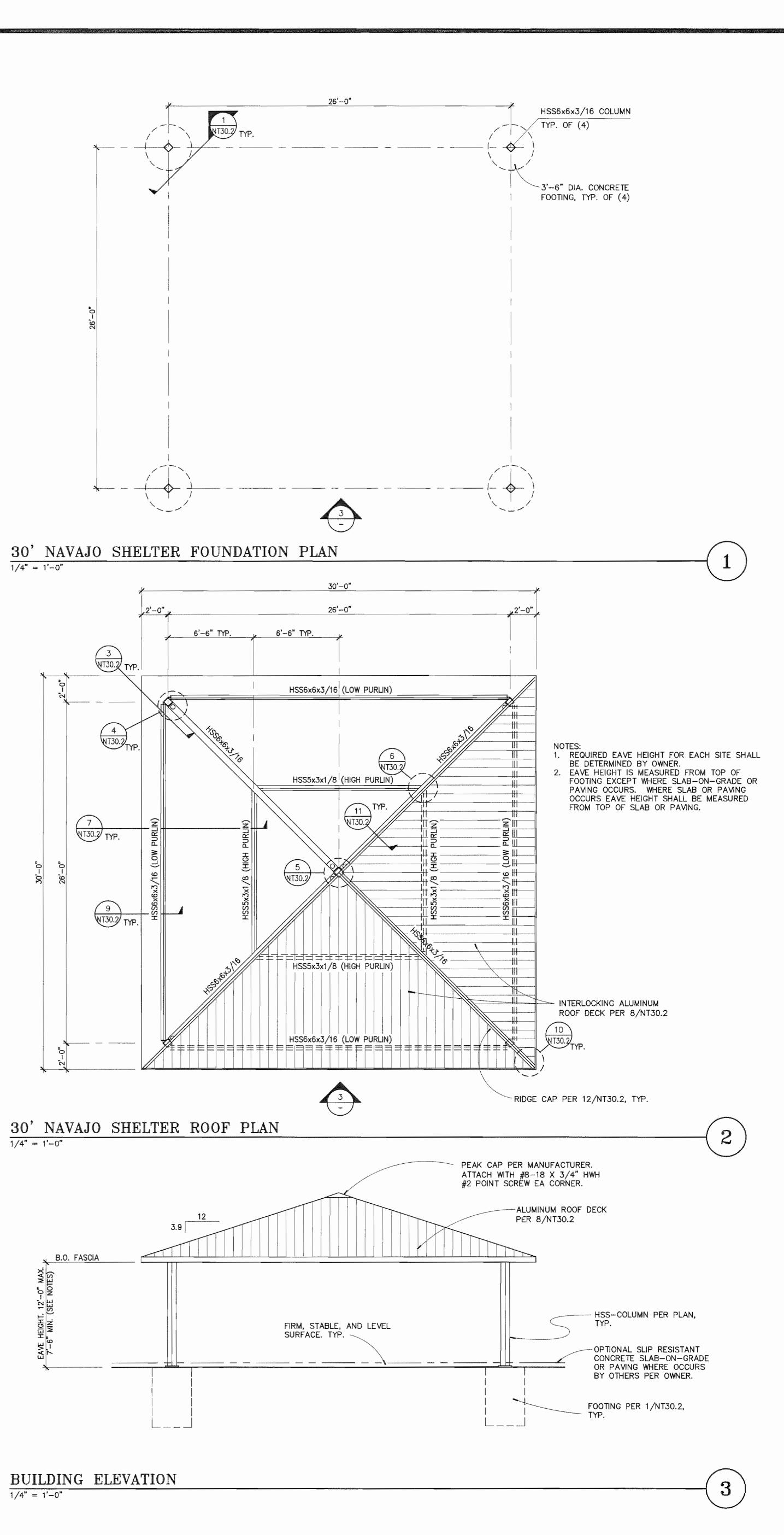
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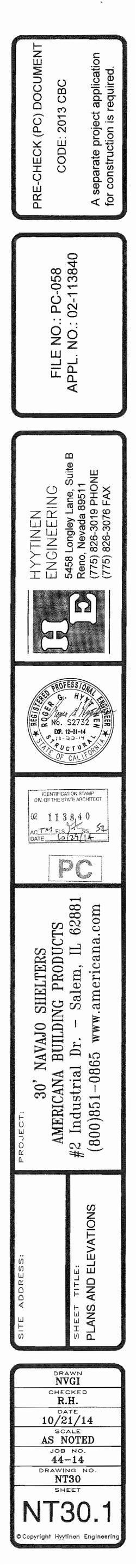
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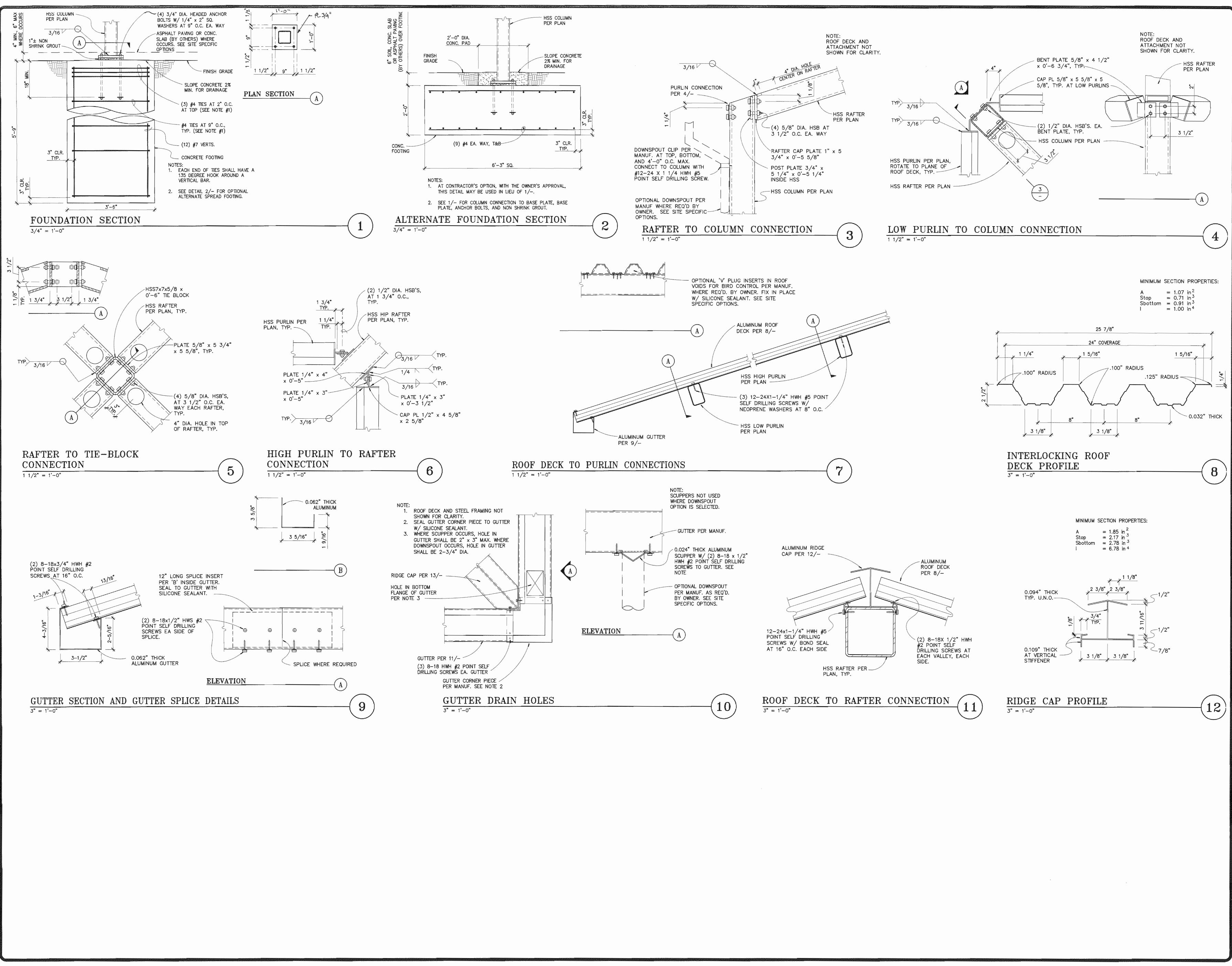






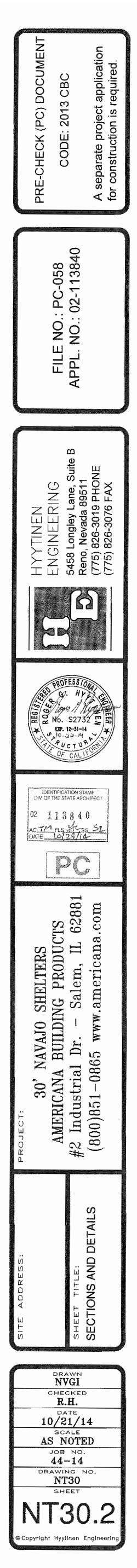






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## **Geotechnical Engineering Report**

Proposed Horticulture Expansion Solano Community College District, Fairfield Campus 4000 Suisun Valley Road Fairfield, California

> December 22, 2015 Terracon Project No. NB155061

Prepared for: Solano Community College District Fairfield, California

> Prepared by: Terracon Consultants, Inc. Sacramento, California



December 22, 2015



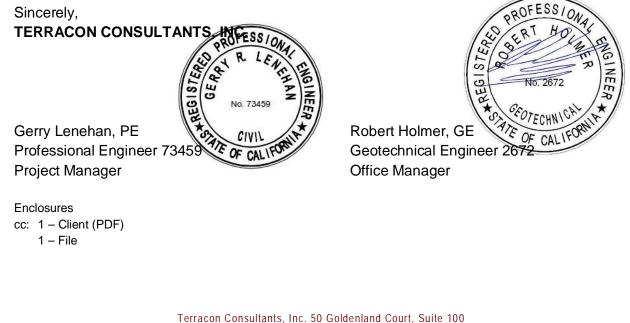
Solano Community College District 360 Campus Lane, suite 203 Fairfield, CA 94534

- Attn: Mr. John Pranys, Sr. Project Engineer P: (707) 863-7869 C: (916) 208-2197 E: john.pranys@solano.edu
- Re: Geotechnical Engineering Report Proposed Horticulture Expansion Solano Community College District, Fairfield Campus 4000 Suisun Valley Road Fairfield, California Terracon Project No. NB155061

Dear Mr. Pranys:

Terracon Consultants, Inc. (Terracon) has completed the geotechnical engineering report for the above referenced project. This study was performed in general accordance with our proposal dated October 5, 2015 with proposal number PNB150339. This report presents the findings of the subsurface exploration and provides geotechnical recommendations concerning earthwork and the design and construction of the proposed expansion.

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report, or if we may be of further service, please contact us.



P [949] 261 0051 F [949] 261 6110 terracon.com



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5.0	GENE		OMMENTS16		

#### **APPENDIX A – FIELD EXPLORATION**

Exhibit A-1	Site Location Plan
Exhibit A-2	Boring Location Diagram
Exhibit A-3	Field Exploration Description
Exhibits A-4 to A-6	Boring Logs

#### **APPENDIX B – LABORATORY TESTING**

Exhibit B-1	Laboratory Test Description
Exhibit B-2	Atterberg Limits Results
Exhibit B-2 to B-3	Grain Size Distribution

#### **APPENDIX C – SUPPORTING DOCUMENTS**

Exhibit C-1General NotesExhibit C-2Unified Soil Classifications



### **EXECUTIVE SUMMARY**

A geotechnical exploration has been performed for the proposed the horticulture expansion at the existing Solano Community College located at 4000 Suisun Valley Road in Fairfield, California. Three (3) borings were drilled to depths of  $11\frac{1}{2}$  to  $51\frac{1}{2}$  feet below ground surface (bgs) within the footprint of the proposed buildings. The geotechnical considerations identified included the following:

- Site Soils: The subsurface soils were generally consistent between borings. The subsurface soils generally consisted of lean clay to sandy lean clay to the maximum depth explored of 51½ feet bgs. Groundwater was encountered at an initial depth of 20 feet bgs and was measured at approximately 16 feet bgs immediately after our exploration was completed.
- **Foundations:** The proposed buildings may be supported by spread footings extending to a depth of at least 24 inches below the lowest adjacent finished soil grade bearing on native soil. The near surface clay soils are not suitable for reuse as engineered fill for this project.
- Seismic Considerations: The 2013 California Building Code (CBC) Seismic Site Classification for this site is D.
- Earthwork: Close monitoring of the construction operations discussed herein will be critical in achieving the design subgrade support. We therefore recommend that Terracon be retained to monitor this portion of the work.

This summary should be used in conjunction with the entire report for design purposes. It should be recognized that details were not included or fully developed in this section, and the report must be read in its entirety for a comprehensive understanding of the items contained herein. The section titled **GENERAL COMMENTS** should be read for an understanding of the report limitations.

### GEOTECHNICAL ENGINEERING REPORT PROPOSED HORTICULTURE EXPANSION SOLANO COMMUNITY COLLEGE, FAIRFIELD CAMPUS 4000 SUISUN VALLEY ROAD SACRAMENTO, CALIFORNIA Terracon Project No. NB155061 December 22, 2015

#### **1.0 INTRODUCTION**

This report presents the results of our geotechnical engineering services performed for the proposed Horticulture Expansion to the existing Solano Community College located at 4000 Suisun Valley Road in Fairfield, California. The Site Location Map (Exhibit A-1) is included in Appendix A of this report. The purpose of these services is to provide information and geotechnical engineering recommendations relative to:

- subsurface soil conditions
- seismic considerations
- earthwork
- exterior concrete sidewalks
- groundwater conditions
- foundation design and construction
- floor slab design and construction
  - retaining walls

Our geotechnical engineering scope of work for this project included the advancement of three (3) borings to a maximum depth of 51½ feet below ground surface (bgs) within the footprint of the proposed buildings.

Logs of borings along with a Boring Location Diagram (Exhibit A-2) are included in Appendix A of this report. The results of the laboratory testing performed on soil samples obtained from the site during the field exploration are included in Appendix B of this report. Descriptions of the field exploration and laboratory testing are included in their respective appendices.

### 2.0 PROJECT INFORMATION

Item	Description				
Site layout	See Appendix A, Exhibit A-1 and A-2: Site Diagram and Boring Location Diagram.				
Structures	The proposed construction will consist of a total of three (3) pre- fabricated buildings, Earthwork and grading will be required at all three locations. The three buildings will include a storage facility (1600 ft ² ), greenhouse (700 ft ² ), and a farmer's stand (1225 ft ² ).				

#### 2.1 **Project Description**

#### **Geotechnical Engineering Report** Proposed Horticulture Expansion Fairfield, California December 22, 2015 Terracon Project No. NB155061



Item	Description			
Construction	Construction will consist of pre-fabricated wood frame buildings founded on a spread footing foundation system with concrete slab on grade floors, with associated asphalt-paved roads and concrete walkways.			
Maximum loads	<ul> <li>Maximum Column Loads: 20-30 kips (assumed)</li> <li>Maximum Wall Loads: less than 2 kips/ft. (assumed)</li> <li>Maximum Floor Loads: less than 100 psf (assumed)</li> </ul>			
Grading	Based upon site topography, cuts and fills on the order of approximately two (2) foot are anticipated to provide a level building pad.			

### 2.2 Site Location and Description

Item	Description				
Location	4000 Suisun Road, Fairfield, California.				
Existing site features	The site is located at the northeastern edge of the Solano Community College campus. The immediate site around the proposed building consists of asphalt paved roadways and parking with structures associated with the campus to the south.				
Surrounding developments	The general location of this site is in Fairfield which is highly developed.				
	North: Solano College Road followed by agricultural land.				
	West: Asphalt-paved parking lot developed by solar car port				
	canopies.				
	South: Solano Community College Campus.				
	East: Solano College Road followed by undeveloped land.				
Current ground cover	The site is covered with grass.				
Existing topography	Site topography is relatively flat with changes in elevation on the order of 1 feet across the site.				
	Based on our review of the State of California Seismic Hazard Zone Maps, the site is not shown to be within an Alquist-Priolo special studies zone for earthquake faults.				
Seismic Hazards	Upon our review of the Association of Bay Area Governments earthquake liquefaction susceptibility maps, the project site si mapped in a 'moderate' area of susceptibility. A liquefaction analysis has been performed as per the 2013 California Building Code.				



#### 3.0 SUBSURFACE CONDITIONS

#### 3.1 Geology

The project area is situated within the Coast Range geomorphic province of California. The native soils underlying the site are considered to consist of undifferentiated alluvial deposits (Q_a) as described on the Geologic Map of the area.¹ According to the map, the sediments are late Quaternary in age (2.6 million years ago and present) and consist of pebble gravel, sand, and clay of valley areas. The surficial mapped geology is consistent with the materials encountered throughout the boring depths.

#### 3.2 Typical Subsurface Profile

Specific conditions encountered at the boring locations are indicated on the individual boring logs. Stratification boundaries on the boring logs represent the approximate location of changes in soils types; in-situ, the transition between materials may be gradual. Details for the borings can be found on the attached boring logs.

The site conditions generally encountered are as follows:

Description	Approximate Depth to Bottom of Stratum	Material Encountered	Consistency/Density	
Stratum 1	50½ feet bgs (Maximum Depth of Exploration)	Lean Clay to Sandy Lean Clay	soft to very stiff	

Laboratory tests were conducted on selected soil samples and the test results are presented in Appendix B. The upper soils encountered at the site generally consisted of lean clay to sandy lean clay. The lean clays exhibited medium to high plasticity, and were found to have the following characteristics:

Sample Location	Depth (feet)	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index	< No. 200 Sieve (%)
Boring B-1	5 to 6½	37	20	17	78
Boring B-3	10 to 11½	38	22	16	90
Boring B-3	1 to 2½	39	19	20	72

¹ Helly, E.J., 1979, Preliminary Geologic Map of Cenozoic Deposits of the Davis, Knights Landing, Lincoln, and Fair Oaks quadrangles, California, USGS, Scale 1:62,500



### 3.3 Groundwater

The boreholes were observed while drilling and after completion for the presence and level of groundwater. Groundwater was observed in the boring B-2 while drilling at a depth of approximately 20 feet and at the completion of drilling at a depth of approximately 16 feet. Groundwater was not encountered in borings B-1 or B-3 during our exploration.

Groundwater level fluctuations occur due to seasonal variations in the amount of rainfall, runoff and other factors not evident at the time the borings were performed. Therefore, groundwater levels during construction or at other times in the life of the structure may be higher or lower than the levels indicated on the boring logs.

### 3.4 Seismic Considerations

The site is located in Northern California, which is a seismically active area. The type and magnitude of seismic hazards affecting the site are dependent on the distance to causative faults, the intensity, and the magnitude of the seismic event. The table below indicates the distance of the fault zones and the associated maximum credible earthquake that can be produced by nearby seismic events, as calculated using the USGS Earthquake Hazard Program 2008 interactive deaggregations.

Characteristics and Estimated Earthquakes for Regional Faults										
Fault Name	Approximate Distance to Site	Maximum Considered Earthquake (MCE) Magnitude								
N. San Andreas; SAO+SAN+SAP+SAS	134.3 km	8.03								
Great Valley 7 Char	66.7 km	6.80								
Hunting Creek-Berryessa Char	97.1 km	7.05								

Based on nearby faults within the proximity of the site, the Maximum Considered Earthquake (MCE) peak ground acceleration at the subject site for a 2% Probability of Exceedance in 50 years is expected to be about 0.782g per the ASCE 7-10 standard with March 2013 errata. The site is not located within an Alquist-Priolo Earthquake Fault Zone based on our review of the State Fault Hazard Maps.²

The following table provides the seismic design criteria in accordance with the 2013 California Building Code at the approximate center of the site, obtained from the USGS Earthquake Hazards website (http://geohazards.usgs.gov/designmaps/us/application.php):

² California Department of Conservation Division of Mines and Geology (CDMG), *"Digital Images of Official Maps of Alquist-Priolo Earthquake Fault Zones of California, Southern Region"*, CDMG Compact Disc 2000-003, 2000.



Code Used	Site Classification
2013 California Building Code (CBC) ¹	D ²
Site Latitude	38.2382°
Site Longitude	-121.1183°
S _s Spectral Acceleration for a Short Period	2.059g
S1 Spectral Acceleration for a 1-Second Period	0.727g

1. In general accordance with the 2013 California Building Code, Table 1613.5.2.

2. The 2013 California Building Code requires a site soil profile determination extending a depth of 100 feet for seismic site classification. The current scope requested does not include the required 100 foot soil profile determination. Borings for this report extended to a maximum depth of approximately 51.5 feet and this seismic site class assignment considers that hard native sandy clay continues below the maximum depth of the subsurface exploration. Additional exploration to greater depths could be considered to confirm the conditions below the current depth of exploration. Alternatively, a geophysical exploration could be utilized in order to attempt to justify a more favorable seismic site class.

# 3.5 Liquefaction

Liquefaction is a mode of ground failure that results from the generation of high pore water pressures during earthquake ground shaking, causing loss of shear strength. Liquefaction is typically a hazard where loose sandy soils exist below groundwater. The CGS has designated certain areas within California Bay Area as potential liquefaction hazard zones. These are areas considered at a risk of liquefaction-related ground failure during a seismic event, based upon mapped sufficial deposits and the presence of a relatively shallow water table. The project site is not located within a liquefaction hazard zone as mapped or evaluated by the CGS. However, the Association of Bay Area Governments Resilience Program (ABAG) liquefaction susceptibility map based on United States Geological Survey (USGS) was reviewed and indicated the site has a moderate liquefaction susceptibility.

The consequences of one-dimensional settlement may be largely mitigated by the presence of the thick non-liquefied layer above the potentially liquefiable soils (Ishihara 1985, Naesgaard et al. 1998, Bouckovalas and Dakoulas 2007). It is our opinion that the presence of stiff lean clay and sandy lean clay soils (non-liquefiable layer) found beneath the existing ground surface may act as a bridging layer that redistributes stresses and therefore results in more uniform ground surface settlement if there is a deeper liquefiable soil beneath the 51½ foot depth of our borings. Based on our experience in this area of Fairfield and the soil conditions found at this site, we have concluded that liquefaction is not a potential hazard at this site.



# 4.0 RECOMMENDATIONS FOR DESIGN AND CONSTRUCTION

### 4.1 Geotechnical Considerations

Based on the results of the subsurface exploration, laboratory testing, and our analysis, it is our opinion that the proposed buildings may be supported on spread foundations that bear on firm undisturbed native clay soils. Geotechnical considerations for this project include:

Expansion potential of subgrade soils

# 4.1.1 Expansion Potential of Subgrade Soils

Moderately expansive clay soils are present at this site. This report provides recommendations to help mitigate the effects of soil shrinkage and expansion on buildings supported on the expansive clay soil. However, even if these procedures are followed, some movement and at least minor cracking in the structure should be anticipated. The severity of cracking and other cosmetic damage such as uneven floor slabs will probably increase if any modification of the site results in excessive wetting or drying of the expansive soils. Eliminating the risk of movement and cosmetic distress may not be feasible, but it may be possible to further reduce the risk of movement if more expensive measures are used during construction.

Spread footing foundations should bear at least 24 inches into the native clay soils. Floor slabs and exterior flatwork should bear on at least 18 inches of engineered fill consisting of low volume change material. The onsite native clay soils materials are not suitable for use as engineered fill for this project.

Geotechnical engineering recommendations for foundation systems and other earth connected phases of the project are outlined below. The recommendations contained in this report are based upon the results of field and laboratory testing (which are presented in Appendices A and B), engineering analyses, and our current understanding of the proposed project.

# 4.2 Earthwork

The following presents recommendations for site preparation, excavation, subgrade preparation and placement of engineered fills on the project. The recommendations presented are for the design and construction of earth supported elements including foundations and concrete slabs on grade and are contingent upon following the recommendations outlined in this section. All grading for the structure should incorporate the limits of the proposed structure plus a lateral distance of at least five feet beyond the outside perimeter (the building pad).

Earthwork on the project should be observed and evaluated by Terracon. The evaluation of earthwork should include observation and testing of engineered fill, subgrade preparation,



foundation bearing soils, and other geotechnical conditions exposed during the construction of the project. Such evaluation is considered an extension of this study.

### 4.2.1 Site Preparation

Strip and remove any existing structures, foundations, slabs, trees, and other deleterious materials within the footprint of the proposed construction. Exposed native soils should be free of mounds and depressions which could prevent uniform compaction. Near surface clay soils are not suitable for use as engineered fill for this project.

# 4.2.2 Subgrade Preparation

Floor slabs and exterior flatwork should be supported on a minimum of 18 inches of engineered fill. The moisture content and compaction of subgrade soils should be maintained until foundation and slab construction. The minimum lateral extent of engineered fill should be at least 5 feet wider than the foundation perimeter. The on-site clay soils are not suitable for use as engineered fill.

During grading operations, exposed soils should be proof rolled and approved by the Engineer prior to the placement of engineered fill. Any soft spots, where the Contractor may have difficulty in obtaining the desired compaction, shall be removed and replaced with compacted engineered fill as described in this report.

# 4.2.3 Engineered Fill Material Requirements

All engineered fill materials from any source should be inorganic soils free of vegetation, debris, and fragments larger than three inches in size. Pea gravel or other similar non-cementitious, poorly-graded materials should not be used as fill or backfill without the prior approval of the geotechnical engineer.

Native clay soils are expansive and not suitable to be used as engineered fill. Import materials for use as engineered fill should be pre-approved by our representative during construction.

Import soils for use as compacted engineered fill material within the proposed building areas should conform to low volume change materials as indicated as follows:



#### Percent Finer by Weight (ASTM C 136)

<u>Gradation</u>	(ASTM C 136)
3"	
No. 4 Sieve	
No. 200 Sieve	
Liquid Limit	
Plasticity Index	
Maximum expansive index*	
*ASTM D4829	

Engineered fill should be placed and compacted in horizontal lifts, using equipment and procedures that will produce recommended moisture contents and densities throughout the lift. Fill lifts should not exceed ten inches loose thickness.

# 4.2.4 Compaction Requirements

Recommended compaction and moisture content criteria for engineered fill materials are as follows:

	Per the Modified Proctor Test (ASTM D 1557)							
Material Type and Location	Minimum Compaction	Range of Moistu Compaction A	ure Contents for bove Optimum					
	Requirement (%)	Minimum	Maximum					
Approved import engineered fill soils:								
Beneath foundations:	90	0	+3					
Beneath slabs:	90	0	+3					
Beneath exterior sidewalks:	90	0	+3					
Utility trenches (structural areas):	90	0	+3					
On site Soils:			+3					
Bottom of excavation receiving fill:	90	0	+3					
Miscellaneous backfill:	90	0	+3					
Utility trenches (Landscape areas):	90	0	+3					
Beneath asphalt pavements:	95	0	+3					
Beneath concrete pavements:	95	0	+3					
Aggregate base (beneath pavements):	95	0	+3					



# 4.2.5 Grading and Drainage

All final grades must provide effective drainage away from the buildings during and after construction. Water permitted to pond next to the building can result in greater soil movements than those discussed in this report. These greater movements can result in unacceptable differential movements, cracks, and leaks. Estimated movements described in this report are based on effective drainage for the life of the structure and cannot be relied upon if effective drainage is not maintained.

Exposed ground should be sloped at least 2 percent away from the building extending a minimum of 5 feet beyond the perimeter of the building. After building construction and landscaping, we recommend the Civil Engineer/Surveyor verify final grades to document that effective drainage has been achieved. Grades around the structure should also be periodically inspected and adjusted as necessary, as part of the structure maintenance program.

Planters located within 10 feet of the structure should be self-contained to prevent water accessing the building and pavement subgrade soils. Locate sprinkler mains and spray heads a minimum of 5 feet away from the building lines. Collect roof runoff in drains or gutters. Discharge roof drains and downspouts onto pavements which slope away from the building or extend down spouts a minimum of 10 feet away from the structure.

Downspouts, roof drains or scuppers should discharge into splash blocks or extensions when the ground surface beneath such features is not protected by exterior slabs or paving. Sprinkler systems should not be installed within 5 feet of foundation walls. Landscaped irrigation adjacent to the foundation systems should be minimized or eliminated.

# 4.2.6 Earthwork Construction Considerations

Based upon the subsurface conditions determined from the geotechnical exploration, subgrade soils exposed during construction are anticipated to be relatively workable. The workability of the subgrade may be affected by precipitation, repetitive construction traffic or other factors. If unworkable conditions develop, workability may be improved by scarifying and drying. If the construction schedule does not allow for scarifying and drying by aeration in place, the contractor may utilize dry crushed rock materials to stabilize wet subgrade materials. If soil stabilization is needed, Terracon should be consulted to evaluate the situation as needed.

Upon completion of filling and grading, care should be taken to maintain the subgrade moisture content. Construction traffic over the completed subgrade should be avoided to the extent practical. The site should also be graded to prevent ponding of surface water on the prepared subgrades or in excavations. If the subgrade should become desiccated, saturated, or disturbed, the affected material should be removed or these materials should be scarified, moisture conditioned, and re-compacted.

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The contractor is responsible for designing and constructing stable, temporary excavations (including utility trenches) as required to maintain stability of both the excavation sides and bottom. Excavations should be sloped or shored in the interest of safety following local and federal regulations, including current OSHA excavation and trench safety standards.

The geotechnical engineer should be retained during the construction phase of the project to observe earthwork and to perform necessary tests and observations during subgrade preparation; proof-rolling; placement and compaction of controlled compacted fills; backfilling of excavations to the completed subgrade.

We recommend that the earthwork portion of this project be completed during extended periods of dry weather if possible. If earthwork is completed during the wet season it may be necessary to take extra precautionary measures to protect subgrade soils. Wet season earthwork may require additional mitigative measures beyond that which would be expected during the drier summer and fall months. This could include diversion of surface runoff around exposed soils and draining of ponded water on the site. Once subgrades are established, it may be necessary to protect the exposed subgrade soils from construction traffic.

# 4.3 Foundations

In our opinion, the proposed building can be supported by a shallow, spread footing foundation system bearing on native soils with footings extending a minimum of 24 inches below lowest adjacent grade. Design recommendations for shallow foundations for the proposed structure are presented in the following paragraphs.

# 4.3.1 Foundation Design Recommendations

DESCRIPTION	RECOMMENDATION					
Foundation Type	Conventional Shallow Spread Footings					
Bearing Material	Native undisturbed soil					
Allowable Bearing Pressure	2,200 psf					
Minimum Plan View Dimensions	Walls: 12 inches; Columns: 24 inches					
Minimum Embedment Below Finished Grade	24 inches					
Total Estimated Settlement	1-inch					
Lateral Resistance	Passive: 300 pcf					
	Coefficient of Friction: 0.30					
Estimated Differential Settlement	1/2 inch over 40 feet					

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# 4.3.2 Foundation Construction Considerations

Finished grade is defined as the lowest adjacent grade within five feet of the foundations. The allowable foundation bearing pressures apply to dead loads plus design live load conditions. The design bearing pressure may be increased by one-third when considering total loads that include transient conditions, such as wind or seismic. The weight of the foundation concrete below grade may be neglected in dead load computations. Passive and friction may be combined to resist lateral loads provided the passive resistance is reduced by half.

Total and differential settlements should not exceed predicted values, provided that:

- Foundations are constructed as recommended, and
- Essentially no changes occur in water contents of foundation soils.

Additional foundation movements could occur if water from any source infiltrates the foundation soils; therefore, proper drainage should be provided in the final design and during construction.

Footings and foundations should be reinforced as necessary to reduce the potential for distress caused by differential foundation movement.

Foundation excavations and bearing soils should be observed by the geotechnical engineer. If the soil conditions encountered differ significantly from those presented in this report, then supplemental recommendations will be required.

The base of all foundation excavations should be free of water, loose soil, and gravel prior to placing concrete. Concrete should be placed soon after excavating and placement of engineered fill to reduce bearing soil disturbance. Should the soils at bearing level become excessively dry, disturbed, or saturated, the affected soil should be removed prior to placing concrete. In addition, as previously described, unsuitable soils should be completely removed from any proposed construction areas prior to construction. We recommend that Terracon be retained to observe and test the soil foundation bearing materials exposed in the over excavation.



# 4.4 Floor Slab

### 4.4.1 Design Recommendations

Item	Description
Floor slab support ¹	At least 18 inches of engineered fill consisting of low volume change material.
Modulus of subgrade reaction	150 pounds per square inch per inch (psi/in) (The modulus was obtained based on our experience with similar subgrade conditions.) ²
Aggregate base course/capillary break	4-inches of crushed, washed ³ / ₄ -inch gravel; or, 6-inches of compacted Aggregate Base (Caltrans Class 2)

1. Upon completion of grading operations in the building area, the recommended subgrade moisture content and density should be maintained to construction of the building floor slabs.

2. This value is for a small load area (1 sq. ft. or less) such as for forklift wheel loads or point loads and should be adjusted for large loaded areas.

The use of a vapor retarder should be considered beneath concrete slabs on grade that will be covered with wood, tile, carpet or other moisture sensitive or impervious coverings, or when the slab will support equipment sensitive to moisture. When conditions warrant the use of a vapor retarder, the slab designer should refer to ACI 302 and/or ACI 360 for procedures and cautions regarding the use and placement of a vapor retarder.

In areas of exposed concrete, control joints should be saw-cut into the slab after concrete placement in accordance with ACI Design Manual, Section 302.1R-37 8.3.12 (tooled control joints are not recommended). To control the width of cracking (should it occur), continuous slab reinforcement should be considered in exposed concrete slabs.

# 4.4.2 Floor Slab Construction Considerations

Interior trench backfill placed beneath slabs should be compacted in accordance with recommendations outlined in the Earthwork section of this report. Other design and construction considerations, as outlined in the ACI Design Manual, Section 302.1R are recommended.

On most project sites, the site grading is generally accomplished early in the construction phase. However as construction proceeds, the subgrade may be disturbed due to utility excavations, construction traffic, desiccation, rainfall, etc. As a result, the floor slab subgrade may not be suitable for placement of base rock and concrete and corrective action will be required.

We recommend the area underlying the floor slab be rough graded and then thoroughly proofrolled with a loaded tandem axel dump truck prior to final grading and placement of base rock. Particular attention should be paid to high traffic areas that were rutted and disturbed earlier and to areas where backfilled trenches are located. Areas where unsuitable conditions are located should be repaired by removing and replacing the affected material with properly compacted fill.



All floor slab subgrade areas should be moisture conditioned and properly compacted to the recommendations in this report immediately prior to placement of the base rock and concrete.

# 4.5 Lateral Earth Pressures

For on-site native soils and fill materials, or imported engineered fill materials above any free water surface, recommended equivalent fluid pressures for foundation elements are:

ITEM	Onsite Soils	Engineered Fill Soils
Active Case (psf/ft)	50	40
Passive Case (psf/ft)	300	400
At-Rest Case (psf/ft)	65	55
Coefficient of Friction	0.30	0.40

The lateral earth pressures herein do not include any factor of safety and are not applicable for submerged soils/hydrostatic loading. These values assume a level backfill. Additional recommendations may be necessary if such conditions are to be included in the design.

Fill against foundation and retaining walls should be compacted to densities recommended in the Earthwork section of this report. Compaction of each lift adjacent to walls should be accomplished with hand-operated tampers or other lightweight compactors.

### 4.6 Pavements

### 4.6.1 Subgrade Preparation

On most project sites, the site grading is accomplished relatively early in the construction phase. Fills are placed and compacted in a uniform manner. However, as construction proceeds, excavations are made into these areas, rainfall and surface water saturates some areas, heavy traffic from concrete trucks and other delivery vehicles disturbs the subgrade and many surface irregularities are filled in with loose soils to improve trafficability temporarily. As a result, the pavement subgrades, initially prepared early in the project, should be carefully evaluated as the time for pavement construction approaches.

We recommend the moisture content and density of the top 10 inches of the subgrade be evaluated and the pavement subgrades be proof rolled within two days prior to commencement of actual paving operations. Areas not in compliance with the required ranges of moisture or density should be moisture conditioned and recompacted. Particular attention should be paid to high traffic areas that were rutted and disturbed earlier and to areas where backfilled trenches are located. Areas where unsuitable conditions are located should be repaired by removing and replacing the materials with properly compacted fills.



After proof rolling and repairing deep subgrade deficiencies, the entire subgrade should be scarified and developed as recommended in Section **4.2** of the **Earthwork** section this report to provide a uniform subgrade for pavement construction. Areas that appear severely desiccated following site stripping may require further undercutting and moisture conditioning. If a significant precipitation event occurs after the evaluation or if the surface becomes disturbed, the subgrade should be reviewed by qualified personnel immediately prior to paving. The subgrade should be in its finished form at the time of the final review

# 4.6.2 Design Considerations

Traffic patterns and anticipated loading conditions were not available at the time that this report was prepared. However, we anticipate that traffic loads will be produced primarily by automobile traffic and occasional delivery and trash removal trucks. The thickness of pavements subjected to heavy truck traffic should be determined using expected traffic volumes, vehicle types, and vehicle loads and should be in accordance with local, city or county ordinances.

Two soil samples were obtained from the near surface soils on the site. Due to similarities in soil type, only one of the two samples was subjected to an R-value test in our laboratory. The approximate locations of the samples are shown on Exhibit A-2 in Appendix A. From the results of the R-value test, an R-value of 5 was obtained.

Pavement performance is affected by its surroundings. In addition to providing preventive maintenance, the civil engineer should consider the following recommendations in the design and layout of pavements:

- Final grade adjacent to parking lots and drives should slope down from pavement edges at a minimum 2%;
- The subgrade and the pavement surface should have a minimum ¼ inch per foot slope to promote proper surface drainage;
- Install pavement drainage surrounding areas anticipated for frequent wetting (e.g., garden centers, wash racks);
- Install joint sealant and seal cracks immediately;
- Seal all landscaped areas in, or adjacent to pavements to reduce moisture migration to subgrade soils;
- Place compacted, low permeability backfill against the exterior side of curb and gutter; and,
- Place curb, gutter and/or sidewalk directly on subgrade soils rather than on unbound granular base course materials.

# 4.6.3 Minimum Pavement Thickness

Assuming the pavement subgrades will be prepared as recommended within this report, the following pavement sections should be considered minimums for this project for the traffic indices assumed in the table below. As more specific traffic information becomes available, we should be contacted to reevaluate the pavement calculations.

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Typical Pavement Section (inches)											
Traffic Area	Alternative	Asphalt Concrete (AC) Surface Course	Portland Cement Concrete (PCC) ¹	Aggregate Base (AB) Course	Total Thickness						
Car Parking	PCC		5.0	4.0	9.0						
Assumed Traffic Index (TI) = 4.0	AC	2.5		7.5	10.0						
Auto Drive Areas	PCC		6.0	4.0	10.0						
Assumed Traffic Index (TI) = 5.0	AC	3.5		8.5	11.0						
Trucks/Heavy Traffic	PCC		6.0	4.0	10						
Assumed Traffic Index (TI) = 6.0	AC	4.5		10.5	15.0						

1. 4,000 psi at 28 days, 4-inch maximum slump and 5 to 7 percent air entrained, 6-sack min. mix. PCC pavements are recommended for trash container pads and in any other areas subjected to heavy wheel loads and/or turning traffic.

These pavement sections are considered minimal sections based upon the expected traffic and the existing subgrade conditions. However, they are expected to function with periodic maintenance and overlays if good drainage is provided and maintained. Base course or pavement materials should not be placed when the surface is wet. Surface drainage should be provided away from the edge of paved areas to minimize lateral moisture transmission into the subgrade.

Subgrade soils beneath all pavements should be scarified, moisture conditioned, and compacted to a minimum depth of 10 inches. All materials should meet the Caltrans Standard Specifications for Highway Construction. Aggregate base materials should meet the gradation and quality requirements of Class 2 Aggregate Base in Caltrans Standard Specifications, latest edition, Sections 25 through 29.

All concrete for rigid pavements should have a minimum flexural strength of 600 psi, and be placed with a maximum slump of four inches. Proper joint spacing will also be required to prevent excessive slab curling and shrinkage cracking. All joints should be sealed to prevent entry of foreign material and dowelled where necessary for load transfer.

# 4.6.4 Pavement Drainage

Pavements should be sloped to provide rapid drainage of surface water. Water allowed to pond on or adjacent to the pavements could saturate the subgrade and contribute to premature pavement deterioration. In addition, the pavement subgrade should be graded to provide positive drainage within the granular base section. Appropriate sub-drainage or connection to a suitable daylight outlet should be provided to remove water from the granular subgrade.



### 4.6.5 Pavement Maintenance

The pavement sections provided in this report represent minimum recommended thicknesses and, as such, periodic maintenance should be anticipated. Therefore preventive maintenance should be planned and provided for through an on-going pavement management program. Maintenance activities are intended to slow the rate of pavement deterioration, and to preserve the pavement investment. Maintenance consists of both localized maintenance (e.g., crack and joint sealing and patching) and global maintenance (e.g., surface sealing). Preventive maintenance is usually the first priority when implementing a pavement maintenance program. Additional engineering observation is recommended to determine the type and extent of a cost effective program. Even with periodic maintenance, some movements and related cracking may still occur and repairs may be required.

# **5.0 GENERAL COMMENTS**

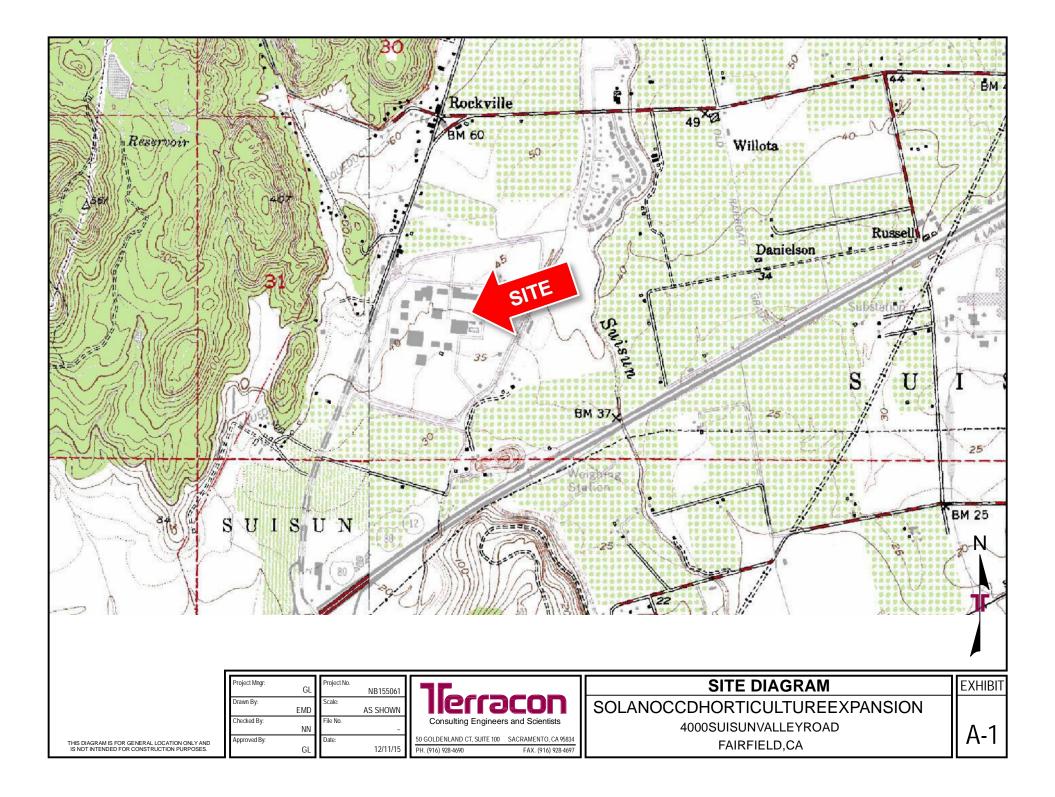
Terracon should be retained to review the final design plans and specifications so comments can be made regarding interpretation and implementation of our geotechnical recommendations in the design and specifications. Terracon also should be retained to provide observation and testing services during grading, excavation, foundation construction and other earth-related construction phases of the project.

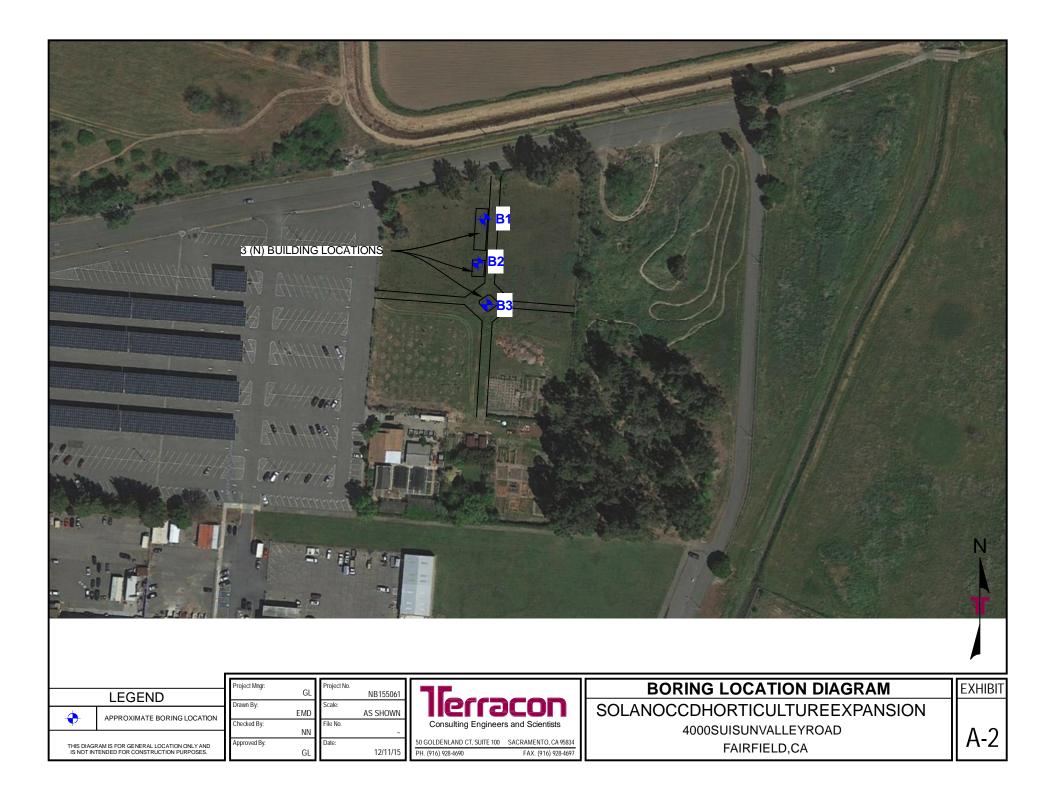
The analysis and recommendations presented in this report are based upon the data obtained from the borings performed at the indicated locations and from other information discussed in this report. This report does not reflect variations that may occur between borings, across the site, or due to the modifying effects of construction or weather. The nature and extent of such variations may not become evident until during or after construction. If variations appear, we should be immediately notified so that further evaluation and supplemental recommendations can be provided.

The scope of services for this project does not include either specifically or by implication any environmental or biological (e.g., mold, fungi, bacteria) assessment of the site or identification or prevention of pollutants, hazardous materials or conditions. If the owner is concerned about the potential for such contamination or pollution, other studies should be undertaken.

This report has been prepared for the exclusive use of our client for specific application to the project discussed and has been prepared in accordance with generally accepted geotechnical engineering practices. No warranties, either expressed or implied, are intended or made. Site safety, excavation support, and dewatering requirements are the responsibility of others. In the event that changes in the nature, design, or location of the project as outlined in this report are planned, the conclusions and recommendations contained in this report shall not be considered valid unless Terracon reviews the changes and either verifies or modifies the conclusions of this report in writing.

APPENDIX A FIELD EXPLORATION







# Field Exploration Description

Our field exploration for this project included performing three (3) test borings to approximate a maximum depth of 50 feet bgs on December 7, 2015. The approximate exploration locations are shown on the Boring Location Diagram, Exhibit A-2. Exploration locations were located in the field by measuring from the existing site features shown on an aerial photo. The exploration locations should only be considered accurate to the degree implied by the means and methods used to define them.

The test borings were advanced with a truck-mounted CME-75 drill rig which utilized 8-inch diameter hollow-stem auger. A continuous log of each boring was recorded during the drilling operations. At selected intervals, samples of the subsurface materials were taken by driving either split-spoon samplers. These logs include visual classifications of the materials encountered during drilling as well as the field engineer's interpretation of the subsurface conditions between samples. Final boring logs included with this report represent the engineer's interpretation of the field logs and include modifications based on laboratory observation and tests of the samples. Groundwater conditions were evaluated in each boring at the time of drilling and upon completion of the field exploration. Groundwater was measured immediately after drilling at a depth of 16 feet in one boring.

Samples of the soils encountered in the borings were obtained using the split barrel sampling procedures described below. The samples were stored in moisture tight containers and transported to our laboratory for further visual classification and testing.

Penetration resistance measurements were obtained by driving the split-spoon and a 2.5-inch outside diameter Modified California sampler into the subsurface materials with a 140-pound hammer falling 30 inches. This test is referred to as the standard penetration test (SPT) and displayed on the logs as an "N" value when the standard 2-inch outer diameter sampler is used. The penetration resistance value is a useful index in estimating the consistency or relative density of materials encountered.

The samples were tagged for identification, sealed to reduce moisture loss, and taken to our laboratory for further examination, testing, and classification. Information provided on the borings logs attached to this report includes soil descriptions, consistency evaluations, borings depths, sampling intervals, relative density and groundwater conditions. The borings were backfilled with soil cuttings and cold patched with asphalt upon completion.

	BORING LOG NO. B1 Page 1 of 1										
PR	OJECT: Solano CCD Horticulture Expansion	CL	IENT: S	Solan Fairfi	no ( eld	Community C	olleg	je Di		-	
SIT	E: 4000 Suisun Valley Road Fairfield, CA		•			, 011					
<b>GRAPHIC LOG</b>	LOCATION See Exhibit A-2 Latitude: 38.2384° Longitude: -122.1184°		DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	LABORATORY TORVANE/HP (tsf)	WATER CONTENT (%)	DRY UNIT WEIGHT (pcf)	ATTERBERG LIMITS	PERCENT FINES
	DEPTH LEAN CLAY WITH SAND (CL), fine grained, medium plasticit brown to brown, very stiff	ty, dark	-			8-13-15	4.25 (HP)	12	99		
	low to medium plasticity, light brown to orange		5			8-12-15	4.5 (HP)	15	98	37-20-17	78
	8.0 LEAN CLAY (CL), silty with fine sand, fine grained, medium p brown to orange, stiff	plasticity,	 								
	11.5 Boring Terminated at 11.5 Feet				X	4-5-5	1.5 (HP)	27	86		
	Stratification lines are approximate. In-situ, the transition may be gradual.				Ha Ha	ammer Type: Automa	tic SPT I	Hammei			
	cement Method: See Exhibit A-3 fo	or description o	of field proced	dures.	No	ites:					
Abando	See Appendix B f procedures and a somment Method: ngs backfilled with neat cement grout upon completion.	additional data (	(if any).								
	WATER LEVEL OBSERVATIONS Groundwater not encountered	rra			Borii	ng Started: 12/7/2015		Borin	g Comp	oleted: 12/7/201	5
		oldenland Ct., S				Rig: CME-75		_	r: Terrac		
		cramento, Calif			Proje	ect No.: NB155061		Exhit	oit:	A-4	

	BORING LOG NO. B2 Page 1 of 2										
PR	OJECT: Solano CCD Horticulture Expansion	nsion	CLIENT:	Solai Fairfi	no C	community (	Colleg	je Di	stric	t	
SIT	E: 4000 Suisun Valley Road Fairfield, CA				iera,	UN					
GRAPHIC LOG	LOCATION See Exhibit A-2 Latitude: 38.2382° Longitude: -122.1184° DEPTH		DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	LABORATORY TORVANE/HP (tsf)	WATER CONTENT (%)	DRY UNIT WEIGHT (pcf)	ATTERBERG LIMITS LL-PL-PI	PERCENT FINES
	LEAN CLAY (CL), silty, fine grained, low to media brown to brown, very stiff	um plasticity, dark	_								
			-	_	X	5-13-17	4.25 (HP)	12	98		
	4.0 <u>SANDY SILTY CLAY (CL-ML)</u> , fine grained, low fight brown, very stiff	to medium plasticity,									
			-	-	M	5-12-15	4.25 (HP)	13	99		
	8.0 <u>LEAN CLAY WITH SAND (CL)</u> , fine grained, med light brown to gray, medium stiff	dium to high plasticit	ty,	-							
			-10		X	2-2-3	1.25 (HP)	27	86	38-22-16	90
			- - - 15-								
	18.0		-			1-6-8	2.25 (HP)	25	98		
	SANDY LEAN CLAY (CL), fine grained, medium to gray, soft	to high plasticity, bro	own 20- -		X	1-1-3 N=4	1.0 (HP)	23	109		75
	very stiff		- - 25-	-			10				
			-	_	XĮ.	2-8-9 N=17	4.0 (HP)	27	110		
	28.0										
	Stratification lines are approximate. In-situ, the transition may be gr	adual.	I.		Ha	mmer Type: Autom	atic SPT	Hammei	r		
Advancement Method:     See Exhibit A-3 for descript       8" Hollow Stem Auger     See Appendix B for descript       Abandonment Method:     See Appendix C for explana       Borings backfilled with neat cement grout upon completion.     See Appendix C for explana			ption of laboratory data (if any).		Not	es:					
$\square$	WATER LEVEL OBSERVATIONS While drilling				Borin	g Started: 12/7/201	5	Borin	ig Comp	leted: 12/7/201	5
$\mathbb{V}$	At completion of drilling	50 Goldenland	<b>ULU</b> I Ct., Ste. 100		-	Rig: CME-75		_	er: Terrad		
		, California		Project No.: NB155061 Exhibit: A-5					A-5		

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL NB155061-LOGS.GPJ TERRACON2015.GDT 12/16/15

	BORING	G LOG N	0.	Bź	2				I	Page 2 of 2	2
PR	<b>OJECT: Solano CCD Horticulture Expansion</b>	CLIENT	: S F	olar airfi	no ( eld	Community ( CA	Colleg	ge Di	stric	t	
SI	TE: 4000 Suisun Valley Road Fairfield, CA		•	ann							
GRAPHIC LOG	LOCATION See Exhibit A-2 Latitude: 38.2382° Longitude: -122.1184°		טבאוח (דנ.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	LABORATORY TORVANE/HP (tsf)	WATER CONTENT (%)	DRY UNIT WEIGHT (pcf)	Atterberg Limits LL-PL-PI	PERCENT FINES
	DEPTH LEAN CLAY (CL), trace sand, fine grained, medium plasticity, b very stiff, with black specs	prown,	_								
		3	-00	×	X	4-7-13 N=20	4.0 (HP)	21	109		94
5		3	- 5 _	5	X	4-10-15 N=25	4.5 (HP)	22	109		
NO WELL NB155061-LOGS.GPJ TERRACON2015.GDT 12/16/15				Ĺ							
IPJ TERRACO	with fine sand, gray mottling	4	-0 	Z	X	5-10-13 N=23	4.5 (HP)	24	94		94
5061-LOGS.G	43.0 SANDY LEAN CLAY (CL), fine grained, stiff, orange mottling		_								
WELL NB15		4	-5-		X	3-7-6 N=13	1.5 (HP)	33	107		
GEO SMART LOG-NO	48.0 <u>LEAN CLAY WITH SAND (CL)</u> , fine grained, medium plasticity brown, very stiff, gray mottling										
	51.5 Boring Terminated at 51.5 Feet				X	6-10-8 N=18	2.25 (HP)	24	108		81
THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT											
EPARATI	Stratification lines are approximate. In-situ, the transition may be gradual.				Ha	ammer Type: Autom	atic SPT	Hamme	r		
Advan 8" H Aband Bor 90 SI 50	Follow Stem Auger See Appendix B fo procedures and ad	description of field p r description of labora ditional data (if any). r explanation of symb	atory		No	tes:					
	WATER LEVEL OBSERVATIONS While drilling				Borii	ng Started: 12/7/2015	5	Borir	ng Comp	leted: 12/7/201	5
	At completion of drilling				Drill	Rig: CME-75		Drille	er: Terrac	con	
THIS	50 Gol	denland Ct., Ste. 100 amento, California			Proje	ect No.: NB155061		Exhil	bit:	A-5	

	BORING LOG NO. B3 Page 1 of 1										
PR	OJECT: Solano CCD Horticulture Expan	CLIENT:	Solan Fairfi	no Co	ommunity (	Colleg	je Di	stric	t		
SIT	E: 4000 Suisun Valley Road Fairfield, CA				ciu,	04					
GRAPHIC LOG	LOCATION See Exhibit A-2 Latitude: 38.2381° Longitude: -122.1183°		DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	LABORATORY TORVANE/HP (tsf)	WATER CONTENT (%)	DRY UNIT WEIGHT (pcf)	ATTERBERG LIMITS LL-PL-PI	PERCENT FINES
	DEPTH <u>LEAN CLAY WITH SAND (CL)</u> , fine to medium, r brown, stiff	nedium plasticity,					4.25				
						7-8-10	(HP)	13	92	39-19-20	72
	fine grained, low plasticity, light brown to orange, v	<i>r</i> ery stiff	-			6-11-15	4.5 (HP)	15	101		
	8.0 <u>SANDY LEAN CLAY (CL)</u> , fine grained, medium to brown with orange, medium stiff	to high plasticity, gra	ay - 10-								
			-			3-2-4	1.5 (HP)	26	88		
	13.0 LEAN CLAY WITH SAND (CL), fine grained, mea stiff	dium to high plasticit	-								
	16.5		- 15			3-4-9	3.25 (HP)	32	89		
	Boring Terminated at 16.5 Feet	adual.			Han	nmer Type: Automa	atic SPT I	Hammer			
	ernent Method: Si ollow Stem Auger	ee Exhibit A-3 for descrip	otion of field proce	edures.	Note	S:					
Abando	onment Method: Single S	ee Appendix B for descri rocedures and additional ee Appendix C for explar obreviations.	data (if any).								
	WATER LEVEL OBSERVATIONS Groundwater not encountered				Boring	Started: 12/7/2015		Borin	g Comp	leted: 12/7/201	5
					Drill Ri	ig: CME-75		Drille	er: R. An	derson	
		l Ct., Ste. 100 o, California		Projec	t No.: NB155061		Exhib	oit:	A-6		

# APPENDIX B LABORATORY TESTING

#### **Geotechnical Engineering Report** Proposed Horticulture Expansion - Fairfield, California December 22, 2015 Terracon Project No. NB155061



#### Laboratory Testing

Samples retrieved during the field exploration were taken to the laboratory for further observation by the project geotechnical engineer and were classified in accordance with the Unified Soil Classification System (USCS) described in Appendix C. At that time, the field descriptions were confirmed or modified as necessary and an applicable laboratory testing program was formulated to determine engineering properties of the subsurface materials.

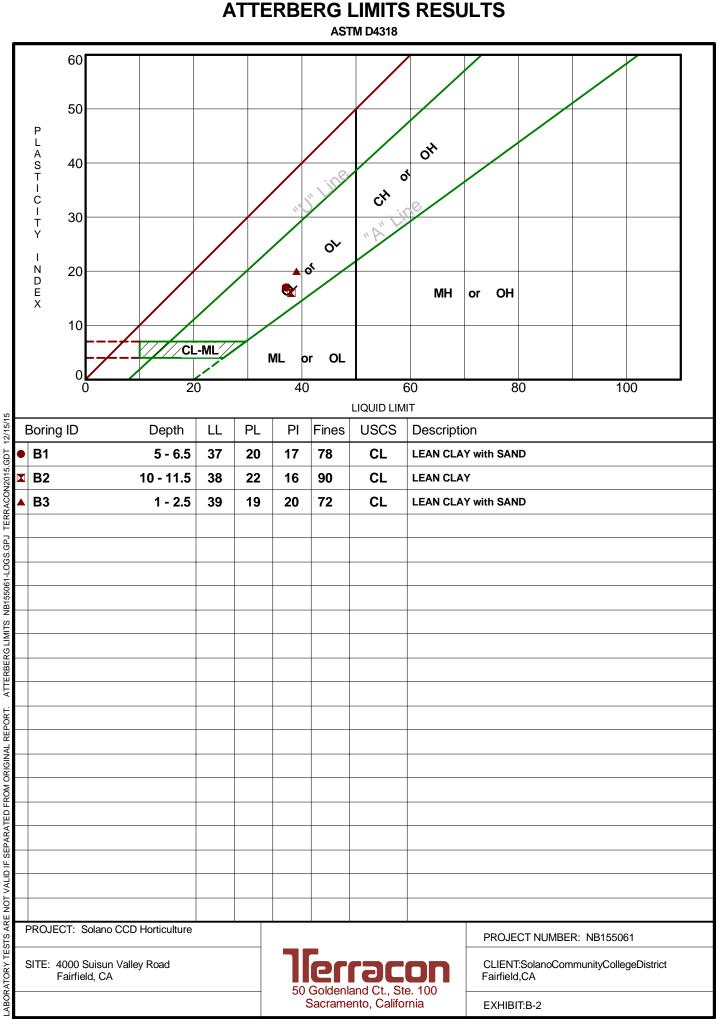
Laboratory tests were conducted on selected soil samples and the test results are presented on the logs of the borings or in the body of the report. The laboratory test results were used for the geotechnical engineering analyses, and the development of engineering, earthwork, and construction recommendations. Laboratory tests were performed in general accordance with the applicable ASTM, local, or other accepted standards.

Selected soil samples obtained from the site were tested for the following engineering properties:

In-situ Water Content

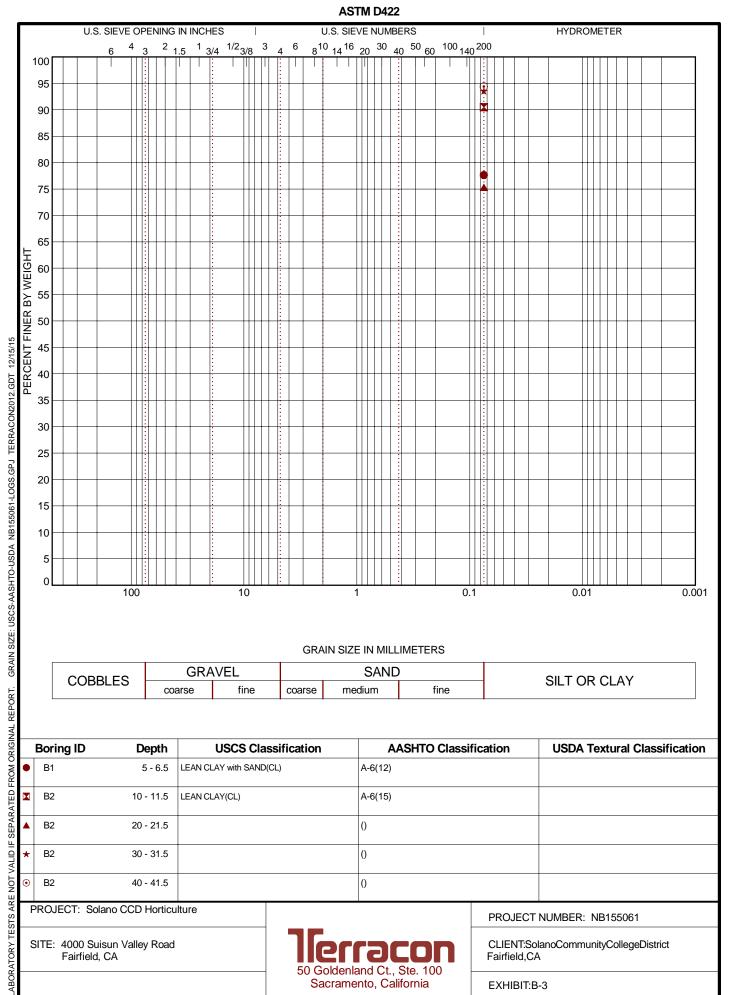
Grain Size Analysis Atterberg Limits 

Unit Weight

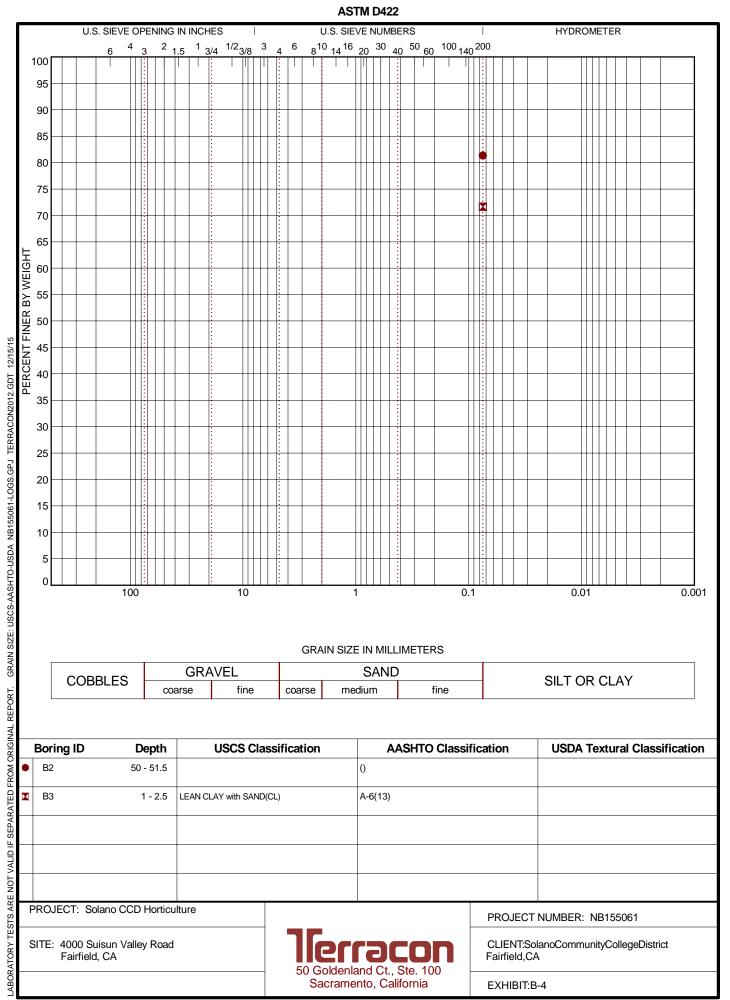


ATTERBERG LIMITS NB155061-LOGS.GPJ TERRACON2015.GDT -ABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT.

# **GRAIN SIZE DISTRIBUTION**



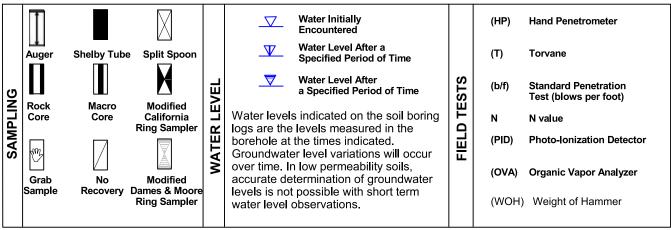
# **GRAIN SIZE DISTRIBUTION**



APPENDIX C SUPPORTING DOCUMENTS

# **GENERAL NOTES**

#### DESCRIPTION OF SYMBOLS AND ABBREVIATIONS



#### **DESCRIPTIVE SOIL CLASSIFICATION**

Soil classification is based on the Unified Soil Classification System. Coarse Grained Soils have more than 50% of their dry weight retained on a #200 sieve; their principal descriptors are: boulders, cobbles, gravel or sand. Fine Grained Soils have less than 50% of their dry weight retained on a #200 sieve; they are principally described as clays if they are plastic, and silts if they are slightly plastic or non-plastic. Major constituents may be added as modifiers and minor constituents may be added according to the relative proportions based on grain size. In addition to gradation, coarse-grained soils are defined on the basis of their in-place relative density and fine-grained soils on the basis of their consistency.

#### LOCATION AND ELEVATION NOTES

Unless otherwise noted, Latitude and Longitude are approximately determined using a hand-held GPS device. The accuracy of such devices is variable. Surface elevation data annotated with +/- indicates that no actual topographical survey was conducted to confirm the surface elevation. Instead, the surface elevation was approximately determined from topographic maps of the area.

	RELATIVE DENSITY OF COARSE-GRAINED SOILS (More than 50% retained on No. 200 sieve.) Density determined by Standard Penetration Resistance Includes gravels, sands and silts.			CONSISTENCY OF FINE-GRAINED SOILS (50% or more passing the No. 200 sieve.) Consistency determined by laboratory shear strength testing, field visual-manual procedures or standard penetration resistance					
TERMS	Descriptive Term (Density)	Standard Penetration or N-Value Blows/Ft.	Ring Sampler Blows/Ft.	Descriptive Term (Consistency)	Unconfined Compressive Strength, Qu, psf	Standard Penetration or N-Value Blows/Ft.	Ring Sampler Blows/Ft.		
1.	Very Loose	0 - 3	0 - 6	Very Soft	less than 500	0 - 1	< 3		
IGTH	Loose	4 - 9	7 - 18	Soft	500 to 1,000	2 - 4	3 - 4		
TRENG	Medium Dense	10 - 29	19 - 58	Medium-Stiff	1,000 to 2,000	4 - 8	5 - 9		
ິ ເ	Dense	30 - 50	59 - 98	Stiff	2,000 to 4,000	8 - 15	10 - 18		
	Very Dense	> 50	<u>&gt;</u> 99	Very Stiff	4,000 to 8,000	15 - 30	19 - 42		
				Hard	> 8,000	> 30	> 42		

#### **RELATIVE PROPORTIONS OF SAND AND GRAVEL**

Descriptive Term(s) of other constituents

Trace

With

Modifier

Percent of Dry Weight < 15 15 - 29 > 30

#### **RELATIVE PROPORTIONS OF FINES**

Descriptive Term(s) of other constituents Trace With Modifier Percent of Dry Weight < 5 5 - 12 > 12

#### **GRAIN SIZE TERMINOLOGY**

Major Component of Sample Boulders Cobbles Gravel Sand Silt or Clay

Over 12 in. (300 mm) 12 in. to 3 in. (300mm to 75mm) 3 in. to #4 sieve (75mm to 4.75 mm) #4 to #200 sieve (4.75mm to 0.075mm Passing #200 sieve (0.075mm)

Particle Size

#### PLASTICITY DESCRIPTION

<u>Term</u> Non-plastic Low Medium High Plasticity Index 0 1 - 10 11 - 30 > 30



	UNIFIED	SOIL CLASS	FICATION SY	<b>STEM</b>		
	Soil Classification					
Criteria for Assigr	Group Symbol	Group Name ^B				
	Gravels: More than 50% of coarse fraction retained on No. 4 sieve	Clean Gravels:	$Cu \ge 4$ and $1 \le Cc \le 3^{E}$		GW	Well-graded gravel ^F
		Less than 5% fines ^c	$Cu < 4$ and/or $1 > Cc > 3^{E}$		GP	Poorly graded gravel F
		Gravels with Fines:	Fines classify as ML or MH		GM	Silty gravel F,G,H
Coarse Grained Soils:		More than 12% fines ^c	Fines classify as CL or CH		GC	Clayey gravel F,G,H
More than 50% retained on No. 200 sieve	Sands: 50% or more of coarse fraction passes No. 4 sieve	<b>Clean Sands:</b> Less than 5% fines ^D	$Cu \ge 6$ and $1 \le Cc \le 3^{E}$		SW	Well-graded sand
01110.200 3000			Cu < 6 and/or 1 > Cc > 3 ^E		SP	Poorly graded sand ¹
		Sands with Fines: More than 12% fines ^D	Fines classify as ML or MH		SM	Silty sand ^{G,H,I}
			Fines classify as CL or CH		SC	Clayey sand G,H,I
	Silts and Clays: Liquid limit less than 50	Inorganic:	PI > 7 and plots on or above "A" line ^J		CL	Lean clay ^{K,L,M}
			PI < 4 or plots below "A" line ^J		ML	Silt ^{K,L,M}
		Organic:	Liquid limit - oven dried	< 0.75	OL	Organic clay K,L,M,N
Fine-Grained Soils:			Liquid limit - not dried			Organic silt K,L,M,O
50% or more passes the No. 200 sieve	Silts and Clays: Liquid limit 50 or more	Inorganic:	PI plots on or above "A" line		СН	Fat clay ^{K,L,M}
			PI plots below "A" line		MH	Elastic Silt K,L,M
		Organic:	Liquid limit - oven dried	< 0.75	ОН	Organic clay K,L,M,P
			Liquid limit - not dried			Organic silt K,L,M,Q
Highly organic soils:	Primarily	PT	Peat			

^A Based on the material passing the 3-inch (75-mm) sieve

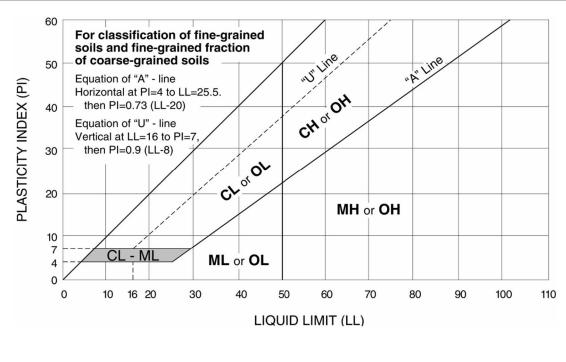
- ^B If field sample contained cobbles or boulders, or both, add "with cobbles or boulders, or both" to group name.
- ^c Gravels with 5 to 12% fines require dual symbols: GW-GM well-graded gravel with silt, GW-GC well-graded gravel with clay, GP-GM poorly graded gravel with silt, GP-GC poorly graded gravel with clay.
- ^D Sands with 5 to 12% fines require dual symbols: SW-SM well-graded sand with silt, SW-SC well-graded sand with clay, SP-SM poorly graded sand with silt, SP-SC poorly graded sand with clay

^E Cu = D₆₀/D₁₀ Cc = 
$$\frac{(D_{30})^2}{D_{10} \times D_{60}}$$

^F If soil contains  $\ge$  15% sand, add "with sand" to group name.

^G If fines classify as CL-ML, use dual symbol GC-GM, or SC-SM.

- ^H If fines are organic, add "with organic fines" to group name.
- If soil contains  $\geq$  15% gravel, add "with gravel" to group name.
- ^J If Atterberg limits plot in shaded area, soil is a CL-ML, silty clay.
- ^K If soil contains 15 to 29% plus No. 200, add "with sand" or "with gravel," whichever is predominant.
- ^L If soil contains ≥ 30% plus No. 200 predominantly sand, add "sandy" to group name.
- ^M If soil contains ≥ 30% plus No. 200, predominantly gravel, add "gravelly" to group name.
- ^N  $PI \ge 4$  and plots on or above "A" line.
- ^o PI < 4 or plots below "A" line.
- ^P PI plots on or above "A" line.
- ^Q PI plots below "A" line.



lferracon